
Attachment 7 – Pedestrian Wind Environment Report, Windtech

Blackwattle Bay

Response to Submissions

June 2022



PEDESTRIAN WIND ENVIRONMENT STUDY

BLACKWATTLE BAY MASTERPLAN, SYDNEY

WD758-22F01 (REV0)- WE REPORT

JUNE 9, 2022

Prepared for:

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DOCUMENT CONTROL

Date	Revision History	Issued Revision	Prepared By (initials)	Instructed By (initials)	Reviewed & Authorised by (initials)
June 9, 2022	Initial.	0	HK	TR	TH

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EXECUTIVE SUMMARY

This report presents the results of a detailed investigation into the wind environment impact of the Blackwattle Bay Masterplan development. Testing was performed at Windtech's boundary layer wind tunnel facility. The wind tunnel has a 3.0m wide working section and a fetch length of 14m, and measurements were taken from 16 wind directions at 22.5 degree increments. Testing was carried out using a 1:400 detailed scale model of the development. The effects of nearby buildings and land topography have been accounted for through the use of a proximity model which represents an area with a radius of 600m. The effect of vegetation was also excluded from the testing to independently assess the design of the building forms within the subject masterplan.

Peak gust and mean wind speeds were determined at selected critical outdoor trafficable locations within and around the subject development. Wind velocity coefficients representing the local wind speeds are derived from the wind tunnel and are combined with a statistical model of the regional wind climate (which accounts for the directional strength and frequency of occurrence of the prevailing regional winds) to provide the equivalent full-scale wind speeds at the site. The wind speed measurements are compared with criteria for pedestrian comfort and safety, based on Gust-Equivalent Mean (GEM) and annual maximum gust winds, respectively.

The majority of the wind conditions within and around the masterplan satisfy the walking comfort and safety criteria, due to how the design of the building forms respond to the prevailing winds to reduce the effect of the north-easterly, southerly, and westerly prevailing winds. Landscaping and other localised wind mitigation measures within and around the site can be implemented at a more detailed design stage.

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INTRODUCTION

A wind tunnel study has been undertaken to determine wind speeds at selected critical outdoor trafficable areas within and around the subject development. The test procedures followed for this wind tunnel study were based on the guidelines set out in the Australasian Wind Engineering Society Quality Assurance Manual (AWES-QAM-1-2019), ASCE 7-16 (Chapter C31), and CTBUH (2013).

A scale model of the development was prepared, including the surrounding buildings and land topography. Testing was performed at Windtech's boundary layer wind tunnel facility. The wind tunnel has a 3.0m wide working section and a fetch length of 14m, and measurements were taken from 16 wind directions at 22.5 degree increments. The wind tunnel was configured to the appropriate boundary layer wind profile for each wind direction. Wind speeds were measured using either Dantec hot-wire probe anemometers or pressure-based wind speed sensors, positioned to monitor wind conditions at critical outdoor trafficable areas of the development.

The model was tested in the wind tunnel without the effect of any forms of wind ameliorating devices such as screens, balustrades, etc., which are not already shown in the architectural drawings. The effect of vegetation was also excluded from the testing. The wind speeds measured during testing were combined with a statistical model of the regional wind climate to provide the equivalent full-scale wind speeds at the site. The measured wind speeds were compared against appropriate criteria for pedestrian comfort and safety, and in-principle treatments have been recommended for any area which was exposed to strong winds. These treatments could be in the form of retaining vegetation that is already proposed for the site, or including additional vegetation, screens, awnings, etc. Note however that, in accordance with the AWES Guidelines (2014), only architectural elements or modifications are used to treat winds which represent an exceedance of the existing wind conditions and exceed the safety limit.

2 WIND TUNNEL MODEL

Wind tunnel testing was carried out using a 1:400 scale model of the development and surroundings. The study model incorporates all necessary architectural features on the façade of the development to ensure an accurate wind flow is achieved around the model, and was constructed using a Computer Aided Manufacturing (CAM) process to ensure that a high level of detail and accuracy is achieved. The model was based on the drawings received May 20, 2022. The effect of nearby buildings and land topography has been accounted for through the use of a proximity model, which represents a radius of 600m from the development site. Photographs of the wind tunnel model are presented in Figures 1. A plan of the proximity model is provided in Figure 2.



Figure 1a: Photograph of the Proposed Wind Tunnel Model (view from the south)



Figure 1b: Photograph of the Proposed Wind Tunnel Model (view from the east)



Figure 1c: Photograph of the Proposed Wind Tunnel Model (view from the north)



Figure 1d: Photograph of the Proposed Wind Tunnel Model (view from the west)

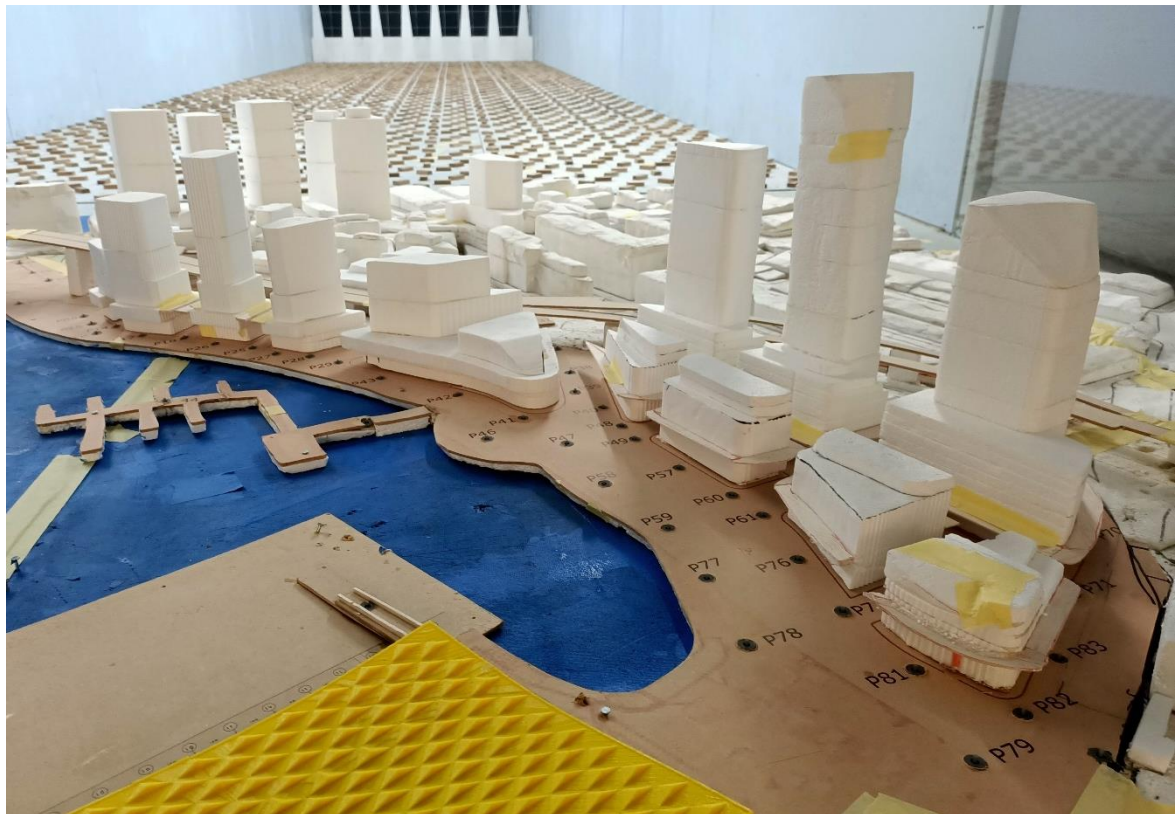


Figure 1e: Photograph of the Proposed Wind Tunnel Model (view from the south-south-east)

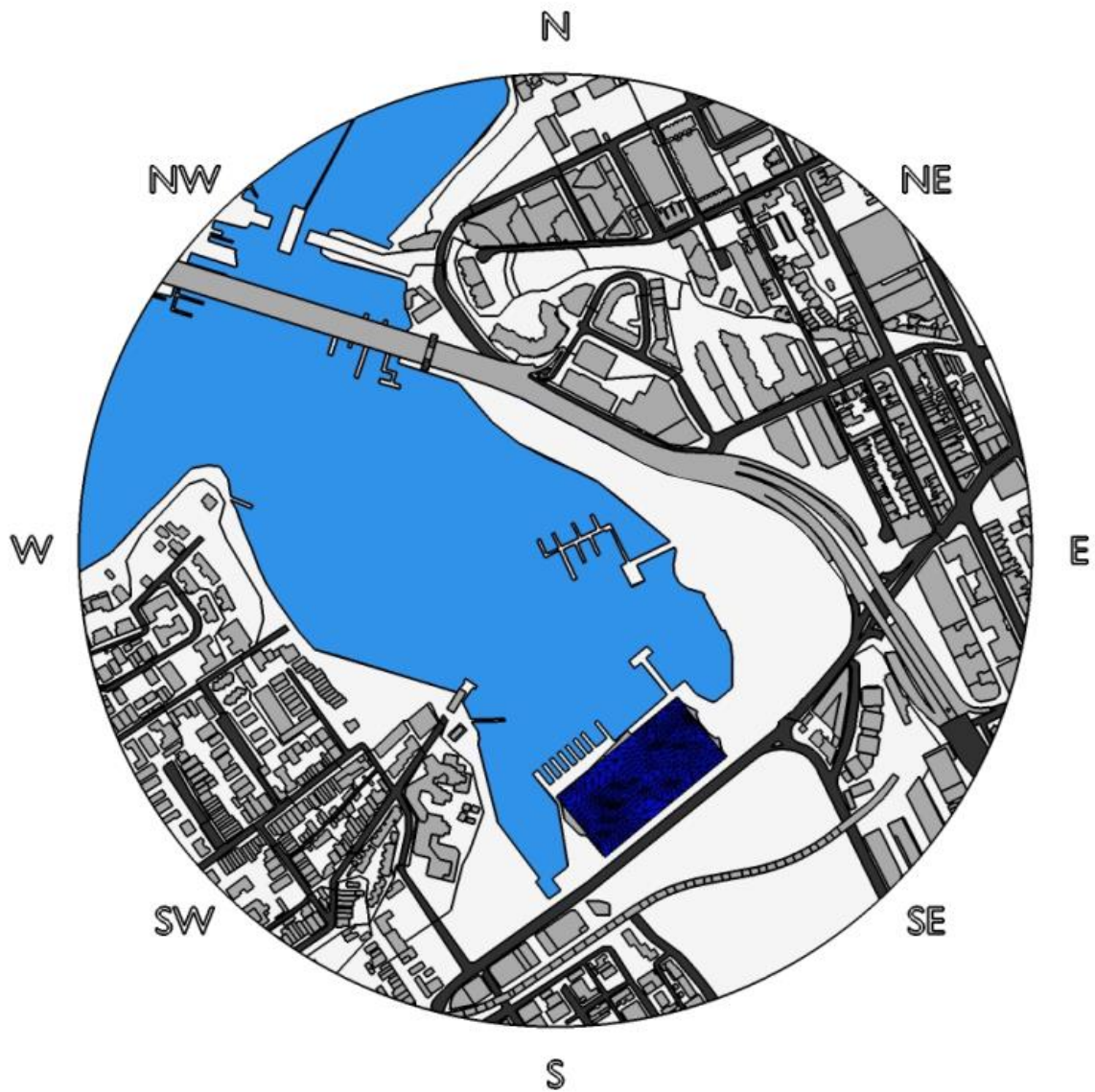


Figure 2: Proximity Model Plan

BOUNDARY LAYER WIND PROFILES AT THE SITE

The roughness of the surface of the earth has the effect of slowing down the wind near the ground. This effect is observed up to the boundary layer height, which can range between 500m to 3km above the earth's surface depending on the roughness of the surface (i.e. oceans, open farmland, etc). Within this range the prevailing wind forms a boundary layer wind profile.

Various wind codes and standards and other publications classify various types of boundary layer wind flows depending on the surface roughness z_0 . Descriptions of typical boundary layer wind profiles, based on D.M. Deaves and R.I. Harris (1978), are summarised as follows:

- Flat terrain ($0.002\text{m} < z_0 < 0.003\text{m}$). Examples include inland water bodies such as lakes, dams, rivers, etc, and the open ocean.
- Semi-open terrain ($0.006\text{m} < z_0 < 0.01\text{m}$). Examples include flat deserts and plains.
- Open terrain ($0.02\text{m} < z_0 < 0.03\text{m}$). Examples include grassy fields, semi-flat plains, and open farmland (without buildings or trees).
- Semi-suburban/semi-forest terrain ($0.06\text{m} < z_0 < 0.1\text{m}$). Examples include farmland with scattered trees and buildings and very low-density suburban areas.
- Suburban/forest terrain ($0.2\text{m} < z_0 < 0.3\text{m}$). Examples include suburban areas of towns and areas with dense vegetation such as forests, bushland, etc.
- Semi-urban terrain ($0.6\text{m} < z_0 < 1.0\text{m}$). Examples include centres of small cities, industrial parks, etc.
- Urban terrain ($2.0\text{m} < z_0 < 3.0\text{m}$). Examples include centres of large cities with many high-rise towers, and also areas with many closely-spaced mid-rise buildings.

The boundary layer wind profile does not change instantly due to changes in the terrain roughness. It can take many kilometres (at least 100km) of a constant surface roughness for the boundary layer wind profile to achieve a state of equilibrium. Hence an analysis of the effect of changes in the upwind terrain roughness is necessary to determine an accurate boundary layer wind profile at the development site location.

The proximity model accounts for the effect of the near field topographic effects as well as the influence of the local built forms. To account for further afield effects, an assessment of the upwind terrain roughness has been undertaken based on the method given in AS/NZS1170.2:2011, using a fetch ranging from 20 to 60 times the study reference height (as per the recommendation by AS/NZS1170.2:2011). An aerial image showing the surrounding terrain is presented in Figure 3 for a range of 4.5km from the edge of the proximity model used for the wind tunnel study. The resulting mean and gust terrain and height multipliers at the site location are presented in Table 1, referenced to the study reference height (which is approximately half the height of the tallest building in the development since typically we are most interested in the wind effects at the ground plane). Details of the boundary layer wind profiles at the site are combined with the regional wind model (see Section 4) to determine the site wind speeds.

Table 1: Approaching Boundary Layer Wind Profile Analysis Summary (at the study reference height)

Wind Sector (degrees)	Terrain and Height Multiplier			Turbulence Intensity I_v	Equivalent Terrain Category (AS/NZS1170.2:2011 naming convention)
	$k_{tr,T=1hr}$ (hourly)	$k_{tr,T=10min}$ (10min)	$k_{tr,T=3s}$ (3sec)		
0	0.89	0.92	1.26	0.138	2.0
30	0.85	0.88	1.24	0.153	2.3
60	0.91	0.95	1.27	0.130	1.8
90	0.80	0.84	1.21	0.173	2.7
120	0.75	0.79	1.18	0.195	3.0
150	0.70	0.74	1.15	0.219	3.2
180	0.71	0.75	1.16	0.213	3.2
210	0.73	0.77	1.17	0.201	3.1
240	0.75	0.79	1.18	0.195	3.0
270	0.78	0.82	1.20	0.179	2.8
300	0.84	0.88	1.23	0.156	2.4
330	0.89	0.93	1.26	0.137	2.0

NOTE: These terrain and height multipliers are to be applied to a basic regional wind speed averaged over 3-seconds. Divide these values by 1.10 for a basic wind speed averaged over 0.2-seconds, 0.69 for a basic wind speed averaged over 10-minutes, or 0.66 for a basic wind speed averaged over 1-hour.

For each of the 16 wind directions tested in this study, the approaching boundary layer wind profiles modelled in the wind tunnel closely matched the profiles listed in Table 1. Plots of the boundary layer wind profiles used for the wind tunnel testing are presented in Appendix D of this report.

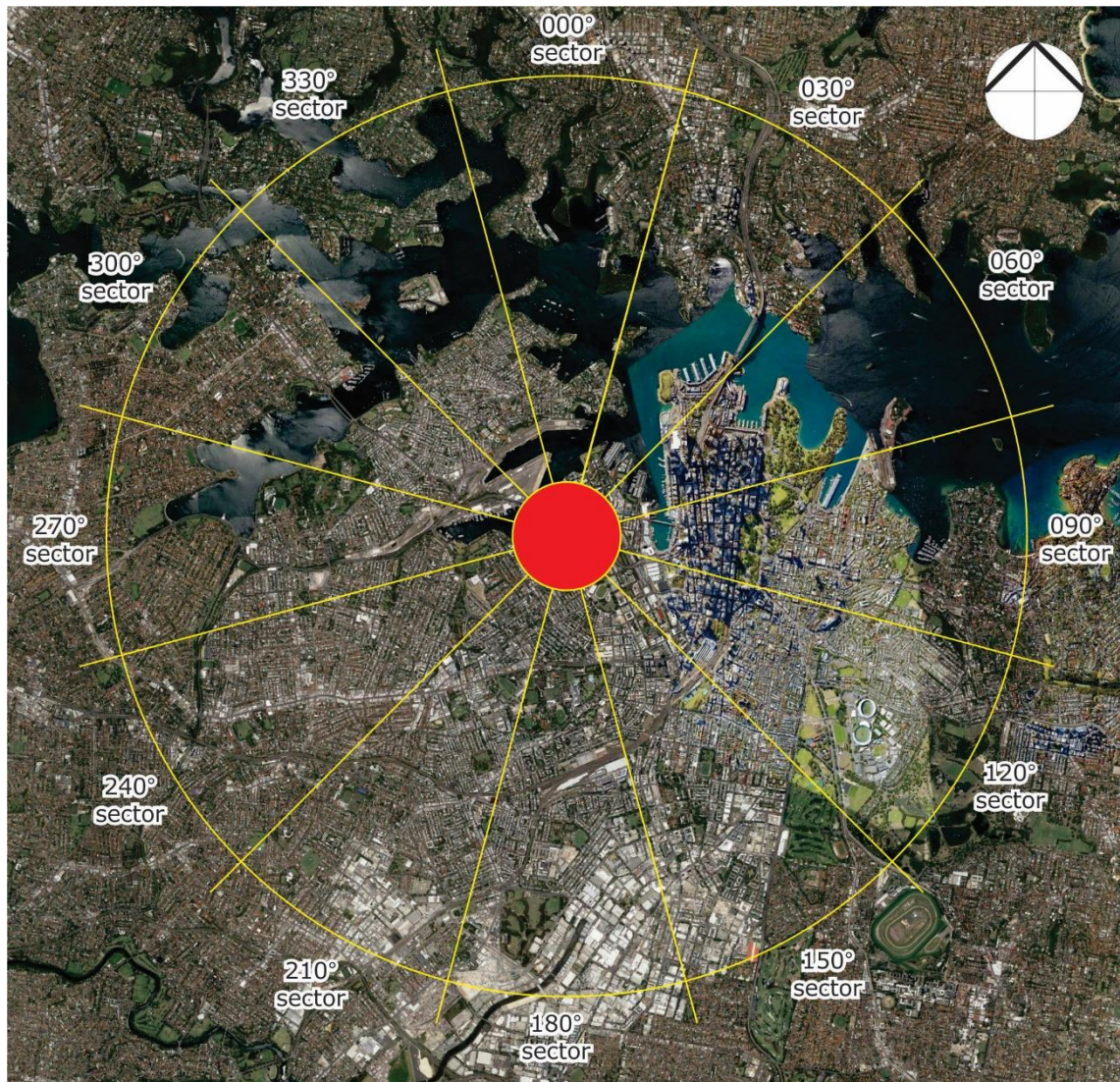


Figure 3: Aerial Image of the Surrounding Terrain (radius of 4.5km from the edge of the proximity model)

4 REGIONAL WIND MODEL

The regional wind model used in this study was determined from an analysis of measured directional mean wind speeds obtained at the meteorological recording station located at Kingsford Smith Airport (Sydney Airport). Data was collected from 1995 to 2016 and corrected so that it represents winds over standard open terrain at a height of 10m above ground for each wind direction. From this analysis, directional probabilities of exceedance and directional wind speeds for the region are determined. The directional wind speeds are summarised in Table 2. The directional wind speeds and corresponding directional frequencies of occurrence are presented in Figure 4.

The data indicates that the southerly winds are by far the most frequent winds for the Sydney region, and are also the strongest. The westerly winds occur most frequently during the winter season for the Sydney region, and although they are typically not as strong as the southerly winds, they are usually a cold wind and hence can be a cause for discomfort for outdoor areas. North-easterly winds occur most frequently occur during the warmer months of the year for the Sydney region, and hence are usually welcomed within outdoor areas since they are typically not as strong as the southerly or westerly winds.

The recurrence intervals examined in this study are for exceedances of 5% (per 90 degree sector) of the pedestrian comfort criteria using Gust-Equivalent Mean (GEM) wind speeds, and annual maximum wind speeds (per 22.5 degree sector) for the pedestrian safety criterion. Note that the 5% probability wind speeds presented in Table 2 are only used for the directional plot presented in Figure 4 and are not used for the integration of the probabilities.

Table 2: Regional Directional Wind Speeds (hourly means, at 10m height in standard open terrain) (m/s)

Wind Direction	5% Exceedance	Annual Maximum
N	5.9	9.9
NNE	9.9	12.9
NE	9.7	12.3
ENE	7.5	10.0
E	6.3	9.3
ESE	6.2	9.1
SE	7.0	10.1
SSE	8.5	12.2
S	10.3	13.9
SSW	10.0	14.1
SW	6.9	11.9
WSW	9.3	13.6
W	9.8	14.4
WNW	8.8	14.3
NW	6.7	12.6
NNW	5.5	10.7

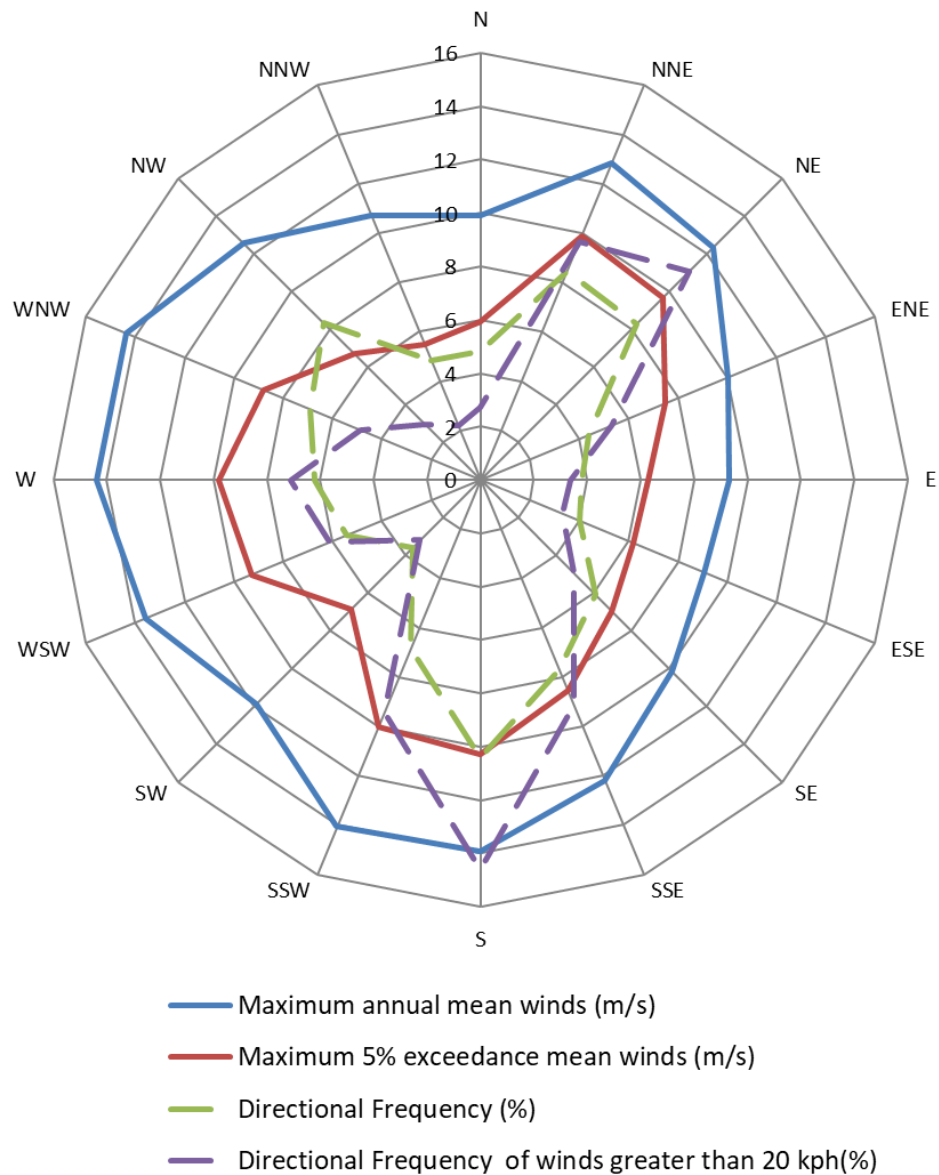


Figure 4: Annual and 5% Exceedance Hourly Mean Wind Speeds, and Frequencies of Occurrence, for the Sydney Region (at 10m height in standard open terrain)

PEDESTRIAN WIND COMFORT AND SAFETY

The acceptability of wind conditions for an area is determined by comparing the measured wind speeds against an appropriate criteria. This section outlines how the measured wind speeds were obtained, the criteria considered for the development, as well as the critical trafficable areas that were assessed and their corresponding criteria designation.

5.1 Measured Wind Speeds

Wind speeds were measured using either Dantec hot-wire probe anemometers or pressure-based wind speed sensors, positioned to monitor wind conditions at critical outdoor trafficable areas of the development. The reference mean free-stream wind speed measured in the wind tunnel, which is at a full-scale height of 200m and measured 3m upstream of the study model.

Measurements were acquired for 16 wind directions at 22.5 degree increments using a sample rate of 1,024Hz. The full methodology of determining the wind speed measurements at the site from either the Dantec Hot-wire probe anemometers or pressure-based wind speed sensors is provided in Appendix B. Based on the results of the analysis of the boundary layer wind profiles at the site (see Section 3), and incorporating the regional wind model (see Section 4), the data sampling length of the wind tunnel test for each wind direction corresponds to a full-scale sample length ranging between 30 minutes and 1 hour. Research by A.W. Rofail and K.C.S. Kwok (1991) has shown that, in addition to the mean and standard deviation of the wind being stable for sample lengths of 15 minutes or more (full-scale), the peak value determined using the upcrossing method is stable for sample lengths of 30 minutes or more.

5.2 Wind Speed Criteria Used for This Study

For this study, the measured wind conditions for the various critical outdoor trafficable areas around the subject development are compared against the criteria presented in the Draft Sydney Development Control Plan 2012 - Central Sydney Planning Review Amendment, which supersedes the criteria detailed in the City of Sydney Development Control Plan 2012 (SDCP2012).

For pedestrian comfort, the Draft Sydney DCP 2012 requires that the hourly mean wind speed, or Gust-Equivalent Mean (GEM) wind speed (whichever is greater for each wind direction), must not exceed 8m/s for walking, 6m/s for standing, and 4m/s for sitting. These are based on a 5% probability of exceedance. For pedestrian safety, the Draft Sydney DCP 2012 defines a safety limit criterion of 24m/s, based on an annual maximum 0.5 second gust wind speed, which applies to all areas.

In accordance with the provisions of the Draft Sydney DCP 2012, the wind speed assessment is undertaken for winds occurring between 6am and 10pm (AEST). A more detailed comparison of published criteria for pedestrian wind comfort and safety is provided in Appendix A.

For this study the measured wind conditions of the selected critical outdoor trafficable areas are compared against two sets of criteria; one for pedestrian safety, and one for pedestrian comfort. The safety criterion is applied to the annual maximum gust winds, and the comfort criteria is applied to Gust Equivalent Mean (GEM) winds. In accordance with ASCE (2003), the GEM wind speed is defined as follows:

$$GEM = \max\left(\bar{V}, \frac{\hat{V}}{1.85}\right) \quad (5.1)$$

where:

\bar{V} is the mean wind speed.

\hat{V} is the gust wind speed.

The criteria considered in this study are summarised in Tables 3 and 4 for pedestrian comfort and safety, respectively. The results of the wind tunnel study are presented in the form of directional plots attached in Appendix C of this report. For each study point there is a plot of the GEM wind speeds using the comfort criteria, and a plot for the annual maximum gust wind speeds using the safety criterion.

Table 3: Pedestrian Comfort Criteria (Draft Sydney DCP 2012)

Classification	Description	Maximum 5% Exceedance GEM Wind Speed (m/s)
Sitting	Outdoor areas that involve seating such as parks, dining areas in restaurants, amphitheatres, etc.	4
Standing	Short duration stationary activities (generally less than 1 hour), including window shopping, waiting areas, etc.	6
Walking	For pedestrian thoroughfares, private swimming pools, most communal areas, private balconies and terraces, etc.	8

Table 4: Pedestrian Safety Criterion (Draft Sydney DCP 2012)

Classification	Description	Annual Maximum Gust Wind Speed (m/s)
Safety	Safety criterion applies to all trafficable areas.	24

5.3 Layout of Study Points

For this study a total of 83 study point locations along the ground level trafficable areas were selected for analysis in the wind tunnel. These are presented in Figure 5 in the form of a marked-up plan. It should be noted that only the most critical outdoor locations of the development have been selected for analysis.

Target Criteria

- City of Sydney DCP 2012 - Central Sydney Planning Review Amendment:
 - Wind Comfort Standard for Walking criterion of 8m/s (5% exceedance) for walking
 - Safety criterion of 24m/s (gust - 0.1% exceedance) for safety

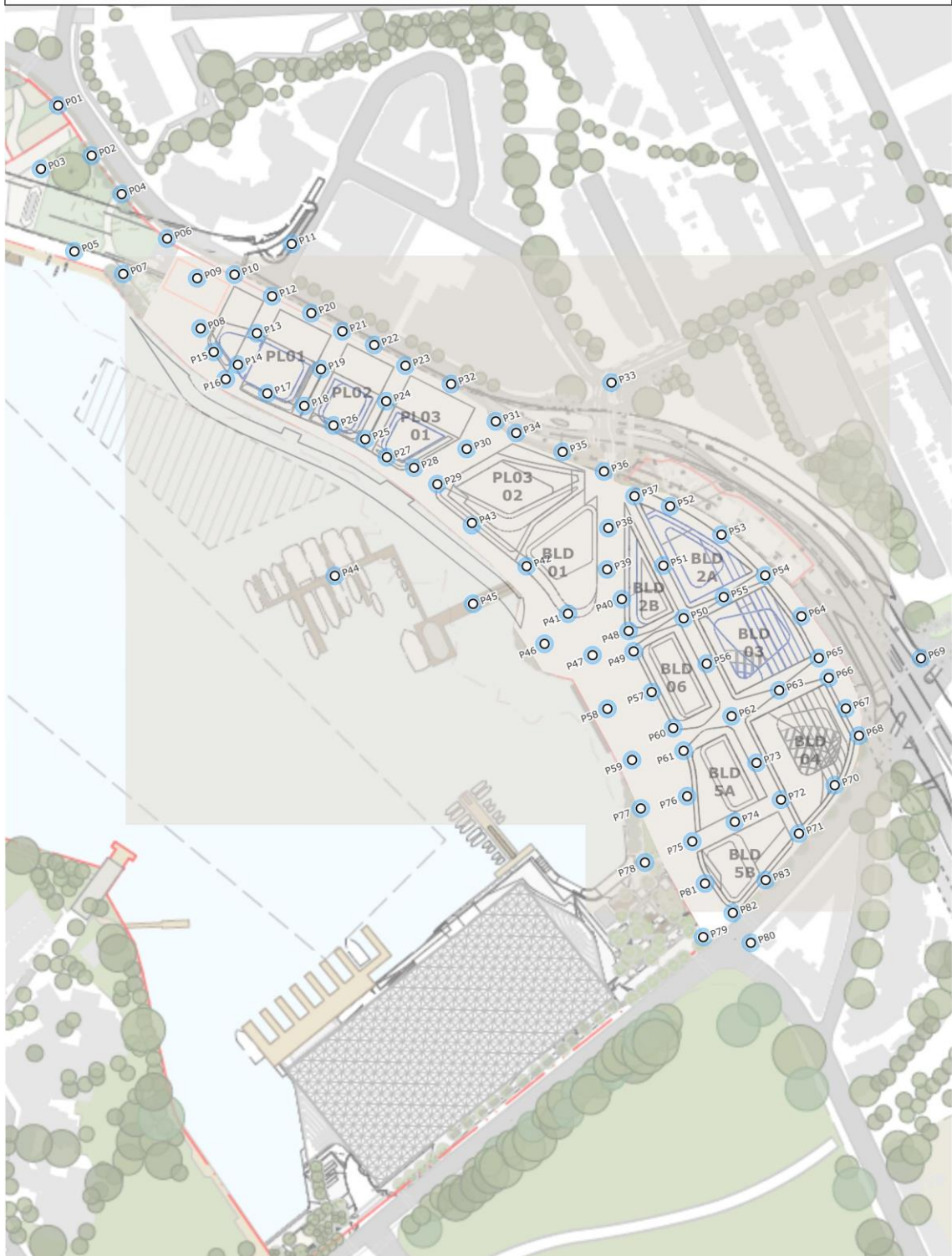


Figure 5: Study Point Locations

RESULTS AND DISCUSSION

The results of the wind tunnel study are presented in the form of directional plots in Appendix C for all study points locations, summarised in Table 5, and shown on marked-up plans in Figures 6, for the configuration shown in Figure 7. The wind speed criteria that the wind conditions should achieve are also listed in Table 5 for each study point location, as well as in Figure 5.

The results of the study indicate that wind conditions for the majority of all ground level trafficable areas will satisfy the walking comfort and safety criteria. Landscaping and other localised wind mitigation measures within and around the site can be implemented at a more detailed design stage, when developing the outdoor usage and final building designs of each of the individual buildings.

Table 5: Wind Tunnel Results Summary

Study Point	GEM (5% exceedance)			Annual Gust			Final Result	Description of Treatment
	Criterion (m/s)	Results (%)	Grade	Criterion (m/s)	Results (m/s)	Grade		
P01	8	5%	Pass	24	24	Pass	Pass	-
P02	8	2%	Pass	24	22	Pass	Pass	-
P03	8	5%	Pass	24	24	Pass	Pass	-
P04	8	2%	Pass	24	21	Pass	Pass	-
P05	8	1%	Pass	24	21	Pass	Pass	-
P06	8	1%	Pass	24	18	Pass	Pass	-
P07	8	2%	Pass	24	22	Pass	Pass	-
P08	8	4%	Pass	24	20	Pass	Pass	-
P09	8	5%	Pass	24	21	Pass	Pass	-
P10	8	3%	Pass	24	23	Pass	Pass	-
P11	8	4%	Pass	24	23	Pass	Pass	-
P12	8	2%	Pass	24	20	Pass	Pass	-
P13	8	7%	Fail	24	23	Pass	Fail	Satisfies safety criterion. Walking comfort can be resolved at a later design stage.
P14	8	6%	Fail	24	23	Pass	Fail	Satisfies safety criterion. Walking comfort can be resolved at a later design stage.
P15	8	3%	Pass	24	21	Pass	Pass	-
P16	8	4%	Pass	24	21	Pass	Pass	-
P17	8	3%	Pass	24	23	Pass	Pass	-
P18	8	4%	Pass	24	20	Pass	Pass	-
P19	8	7%	Fail	24	22	Pass	Fail	Satisfies safety criterion. Walking comfort can be resolved at a later design stage.
P20	8	1%	Pass	24	21	Pass	Pass	-
P21	8	< 1%	Pass	24	16	Pass	Pass	-
P22	8	< 1%	Pass	24	13	Pass	Pass	-
P23	8	< 1%	Pass	24	15	Pass	Pass	-
P24	8	5%	Pass	24	23	Pass	Pass	-

Study Point	GEM (5% exceedance)			Annual Gust			Final Result	Description of Treatment
	Criterion (m/s)	Results (%)	Grade	Criterion (m/s)	Results (m/s)	Grade		
P25	8	4%	Pass	24	19	Pass	Pass	-
P26	8	1%	Pass	24	18	Pass	Pass	-
P27	8	2%	Pass	24	20	Pass	Pass	-
P28	8	7%	Fail	24	22	Pass	Fail	Satisfies safety criterion. Walking comfort can be resolved at a later design stage.
P29	8	7%	Fail	24	23	Pass	Fail	Satisfies safety criterion. Walking comfort can be resolved at a later design stage.
P30	8	15%	Fail	24	24	Pass	Fail	Satisfies safety criterion. Walking comfort can be resolved at a later design stage.
P31	8	3%	Pass	24	22	Pass	Pass	-
P32	8	< 1%	Pass	24	14	Pass	Pass	-
P33	8	< 1%	Pass	24	16	Pass	Pass	-
P34	8	7%	Fail	24	24	Pass	Fail	Satisfies safety criterion. Walking comfort can be resolved at a later design stage.
P35	8	1%	Pass	24	21	Pass	Pass	-
P36	8	4%	Pass	24	21	Pass	Pass	-
P37	8	5%	Pass	24	22	Pass	Pass	-
P38	8	8%	Fail	24	23	Pass	Fail	Satisfies safety criterion. Walking comfort can be resolved at a later design stage.
P39	8	9%	Fail	24	21	Pass	Fail	Satisfies safety criterion. Walking comfort can be resolved at a later design stage.
P40	8	3%	Pass	24	20	Pass	Pass	-
P41	8	1%	Pass	24	20	Pass	Pass	-
P42	8	1%	Pass	24	20	Pass	Pass	-
P43	8	1%	Pass	24	19	Pass	Pass	-
P44	8	2%	Pass	24	23	Pass	Pass	-
P45	8	4%	Pass	24	22	Pass	Pass	-
P46	8	4%	Pass	24	22	Pass	Pass	-
P47	8	2%	Pass	24	20	Pass	Pass	-
P48	8	1%	Pass	24	16	Pass	Pass	-
P49	8	5%	Pass	24	22	Pass	Pass	-
P50	8	7%	Fail	24	21	Pass	Fail	Satisfies safety criterion. Walking comfort can be resolved at a later design stage.
P51	8	1%	Pass	24	18	Pass	Pass	-
P52	8	2%	Pass	24	19	Pass	Pass	-
P53	8	3%	Pass	24	23	Pass	Pass	-
P54	8	2%	Pass	24	20	Pass	Pass	-
P55	8	15%	Fail	24	24	Pass	Fail	Satisfies safety criterion. Walking comfort can be resolved at a later design stage.
P56	8	2%	Pass	24	21	Pass	Pass	-
P57	8	< 1%	Pass	24	16	Pass	Pass	-
P58	8	1%	Pass	24	20	Pass	Pass	-

Study Point	GEM (5% exceedance)			Annual Gust			Final Result	Description of Treatment
	Criterion (m/s)	Results (%)	Grade	Criterion (m/s)	Results (m/s)	Grade		
P59	8	2%	Pass	24	21	Pass	Pass	-
P60	8	3%	Pass	24	21	Pass	Pass	-
P61	8	12%	Fail	24	27	Fail	Fail	Localised screening recommended in-principle. Walking comfort can be resolved at a later design stage.
P62	8	14%	Fail	24	23	Pass	Fail	Satisfies safety criterion. Walking comfort can be resolved at a later design stage.
P63	8	17%	Fail	24	24	Pass	Fail	Satisfies safety criterion. Walking comfort can be resolved at a later design stage.
P64	8	1%	Pass	24	19	Pass	Pass	-
P65	8	5%	Pass	24	21	Pass	Pass	-
P66	8	3%	Pass	24	21	Pass	Pass	-
P67	8	4%	Pass	24	22	Pass	Pass	-
P68	8	11%	Fail	24	24	Pass	Fail	Satisfies safety criterion. Walking comfort can be resolved at a later design stage.
P69	8	< 1%	Pass	24	13	Pass	Pass	-
P70	8	5%	Pass	24	21	Pass	Pass	-
P71	8	3%	Pass	24	21	Pass	Pass	-
P72	8	2%	Pass	24	19	Pass	Pass	-
P73	8	2%	Pass	24	20	Pass	Pass	-
P74	8	2%	Pass	24	21	Pass	Pass	-
P75	8	2%	Pass	24	21	Pass	Pass	-
P76	8	1%	Pass	24	18	Pass	Pass	-
P77	8	2%	Pass	24	20	Pass	Pass	-
P78	8	1%	Pass	24	20	Pass	Pass	-
P79	8	2%	Pass	24	22	Pass	Pass	-
P80	8	< 1%	Pass	24	11	Pass	Pass	-
P81	8	2%	Pass	24	23	Pass	Pass	-
P82	8	2%	Pass	24	22	Pass	Pass	-
P83	8	4%	Pass	24	22	Pass	Pass	-

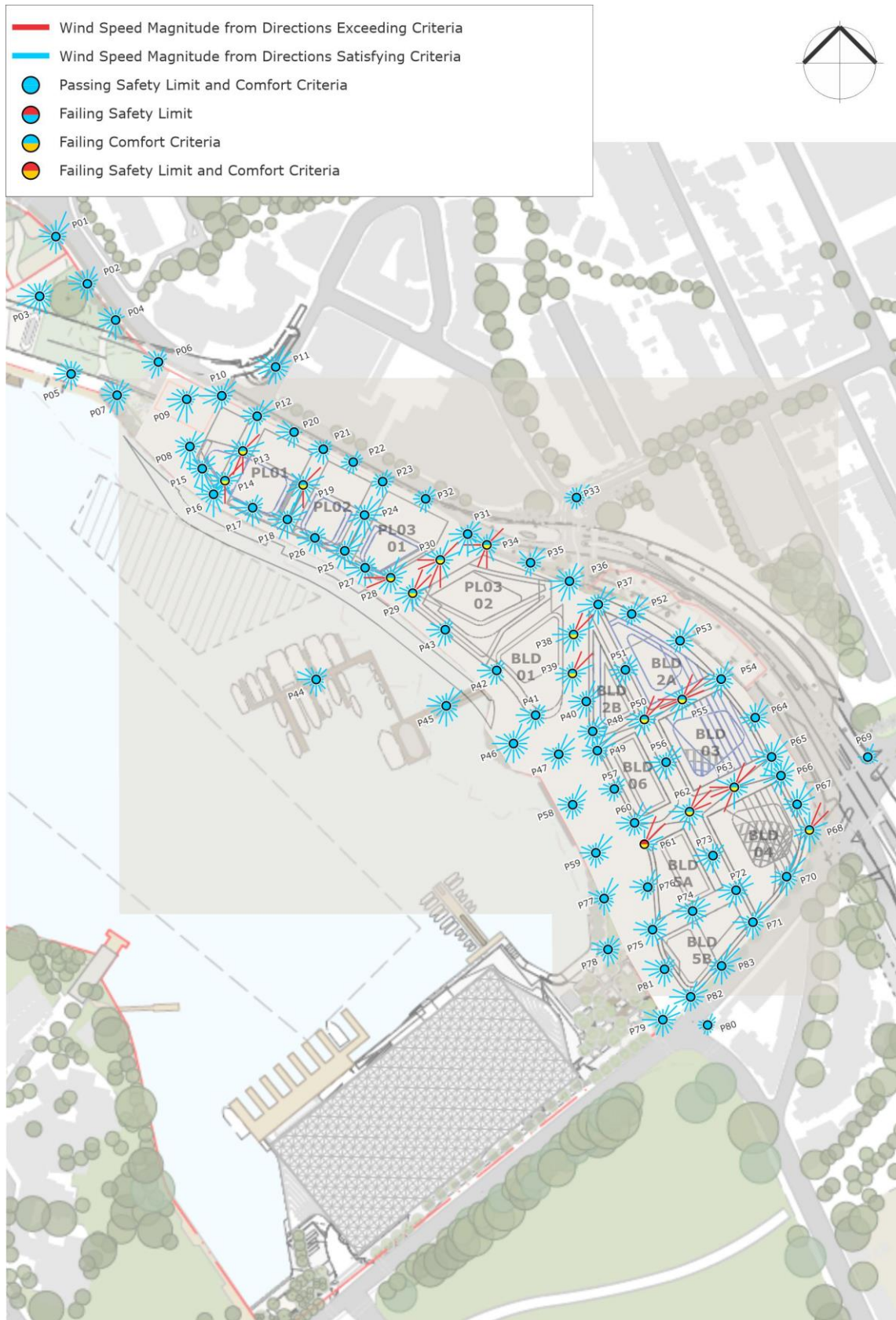


Figure 6: Wind Tunnel Results

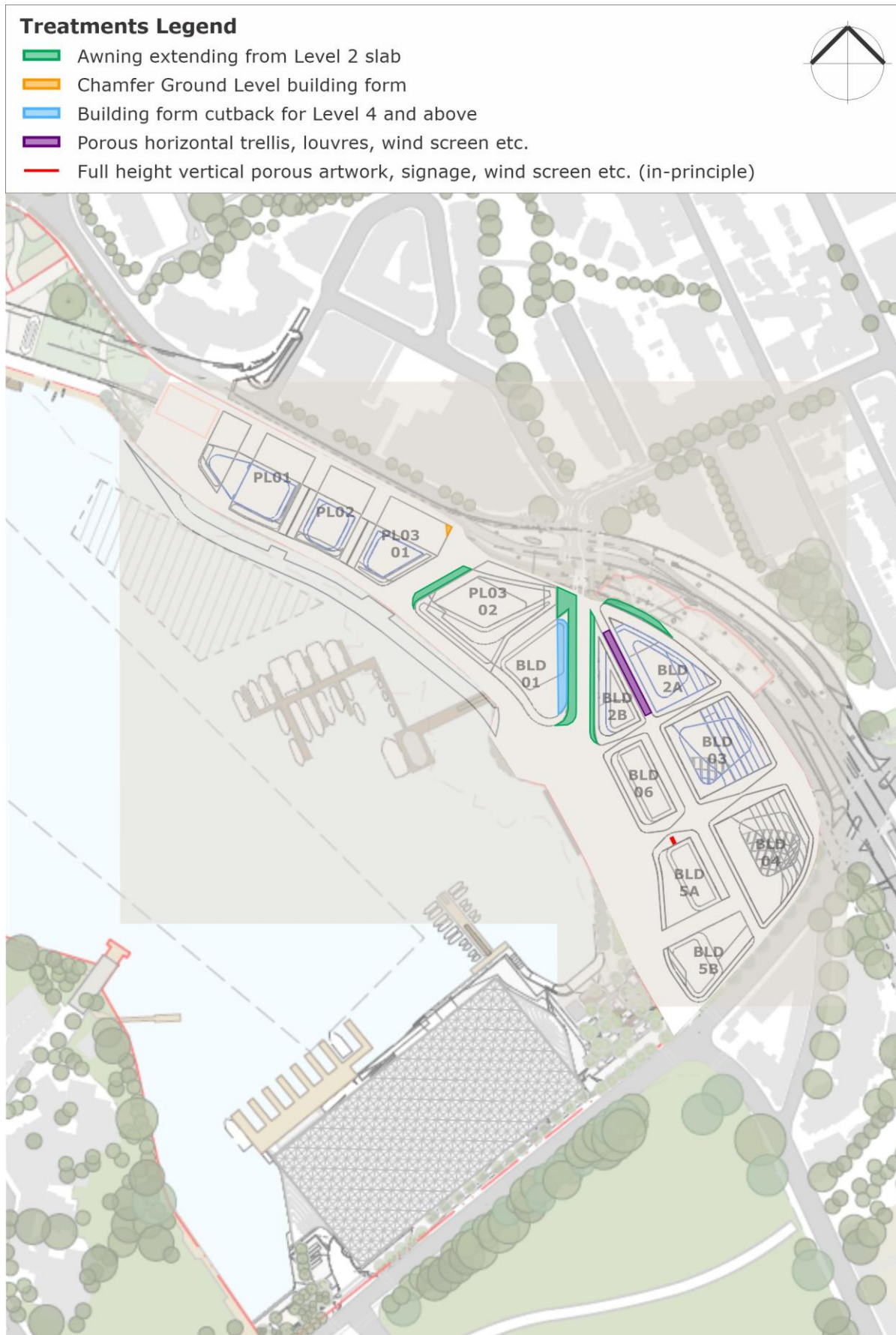


Figure 7: Tested Configuration Scheme

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APPENDIX A PUBLISHED ENVIRONMENTAL CRITERIA

A.1 Wind Effects on People

The acceptability of wind in an area is dependent upon the use of the area. For example, people walking or window-shopping will tolerate higher wind speeds than those seated at an outdoor restaurant. Quantifying wind comfort has been the subject of much research and many researchers, such as A.G. Davenport, T.V. Lawson, W.H. Melbourne, and A.D. Penwarden, have published criteria for pedestrian comfort for pedestrians in outdoor spaces for various types of activities. This section discusses and compares the various published criteria.

A.2 A.D. Penwarden (1973) Criteria for Mean Wind Speeds

A.D. Penwarden (1973) developed a modified version of the Beaufort scale which describes the effects of various wind intensities on people. Table A.1 presents the modified Beaufort scale. Note that the effects listed in this table refers to wind conditions occurring frequently over the averaging time (a probability of occurrence exceeding 5%). Higher ranges of wind speeds can be tolerated for rarer events.

Table A.1: Summary of Wind Effects on People (A.D. Penwarden, 1973)

Type of Winds	Beaufort Number	Hourly Mean Wind Speed (m/s)	Effects
Calm	0	0 - 0.3	
Calm, light air	1	0.3 - 1.6	No noticeable wind
Light breeze	2	1.6 - 3.4	Wind felt on face
Gentle breeze	3	3.4 - 5.5	Hair is disturbed, clothing flaps, newspapers difficult to read
Moderate breeze	4	5.5 - 8.0	Raises dust, dry soil and loose paper, hair disarranged
Fresh breeze	5	8.0 - 10.8	Force of wind felt on body, danger of stumbling
Strong breeze	6	10.8 - 13.9	Umbrellas used with difficulty, hair blown straight, difficult to walk steadily, wind noise on ears unpleasant
Near gale	7	13.9 - 17.2	Inconvenience felt when walking
Gale	8	17.2 - 20.8	Generally impedes progress, difficulty balancing in gusts
Strong gale	9	20.8 - 24.5	People blown over

A.3 A.G. Davenport (1972) Criteria for Mean Wind Speeds

A.G. Davenport (1972) also determined a set of criteria in terms of the Beaufort scale and for various return periods. Table A.2 presents a summary of the criteria based on a probability of exceedance of 5%.

Table A.2: Criteria by A.G. Davenport (1972)

Classification	Activities	5% exceedance Mean Wind Speed (m/s)
Walking Fast	Acceptable for walking, main public accessways.	7.5 - 10.0
Strolling, Skating	Slow walking, etc.	5.5 - 7.5
Short Exposure Activities	Generally acceptable for walking & short duration stationary activities such as window-shopping, standing or sitting in plazas.	3.5 - 5.5
Long Exposure Activities	Generally acceptable for long duration stationary activities such as in outdoor restaurants & theatres and in parks.	0 - 3.5

A.4 T.V. Lawson (1975) Criteria for Mean Wind Speeds

In 1973, T.V. Lawson, while referring to the Beaufort wind speeds of A.D. Penwarden (1973) (as listed in Table A.1), quoted that a Beaufort 4 wind speed would be acceptable if it is not exceeded for more than 4% of the time, and that a Beaufort 6 wind speed would be unacceptable if it is exceeded more than 2% of the time. Later, in 1975, T.V. Lawson presented a set of criteria very similar to those presented in A.G. Davenport (1972) (as listed in Table A.2). These criteria are presented in Table A.3 and Table A.4 for safety and comfort respectively.

Table A.3: Safety Criteria by T.V. Lawson (1975)

Classification	Activities	Annual Mean Wind Speed (m/s)
Safety (all weather areas)	Accessible by the general public.	0 – 15
Safety (fair weather areas)	Private areas, balconies/terraces, etc.	0 – 20

Table A.4: Comfort Criteria by T.V. Lawson (1975)

Classification	Activities	5% exceedance Mean Wind Speed (m/s)
Business Walking	Objective Walking from A to B.	8 - 10
Pedestrian Walking	Slow walking, etc.	6 - 8
Short Exposure Activities	Pedestrian standing or sitting for short times.	4 – 6
Long Exposure Activities	Pedestrian sitting for a long duration.	0 - 4

A.5 W.H. Melbourne (1978) Criteria for Gust Wind Speeds

W.H. Melbourne (1978) introduced a set of criteria for the assessment of environmental wind conditions that were developed for a temperature range of 10°C to 30°C and for people suitably dressed for outdoor conditions. These criteria are presented in Table A.5, and are based on maximum gust wind speeds with a probability of exceedance of once per year.

Table A.5: Criteria by W.H. Melbourne (1978)

Classification	Activities	Annual Gust Wind Speed (m/s)
Limit for Safety	Completely unacceptable: people likely to get blown over.	23
Marginal	Unacceptable as main public accessways.	16 - 23
Comfortable Walking	Acceptable for walking, main public accessways	13 - 16
Short Exposure Activities	Generally acceptable for walking & short duration stationary activities such as window-shopping, standing or sitting in plazas.	10 - 13
Long Exposure Activities	Generally acceptable for long duration stationary activities such as in outdoor restaurants & theatres and in parks.	0 - 10

A.6 Comparison of the Published Wind Speed Criteria

W.H. Melbourne (1978) presented a comparison of the criteria of various researchers on a probabilistic basis. Figure A.1 presents the results of this comparison, and indicates that the criteria of W.H. Melbourne (1978) are comparatively quite conservative. This conclusion was also observed by A.W. Rofail (2007) when undertaking on-site remedial studies. The results of A.W. Rofail (2007) concluded that the criteria by W.H. Melbourne (1978) generally overstates the wind effects in a typical urban setting due to the assumption of a fixed 15% turbulence intensity for all areas. It was observed in A.W. Rofail (2007) that the 15% turbulence intensity assumption is not real and that the turbulence intensities at 1.5m above ground is at least 20% and in a suburban or urban setting is generally in the range of 30% to 60%.

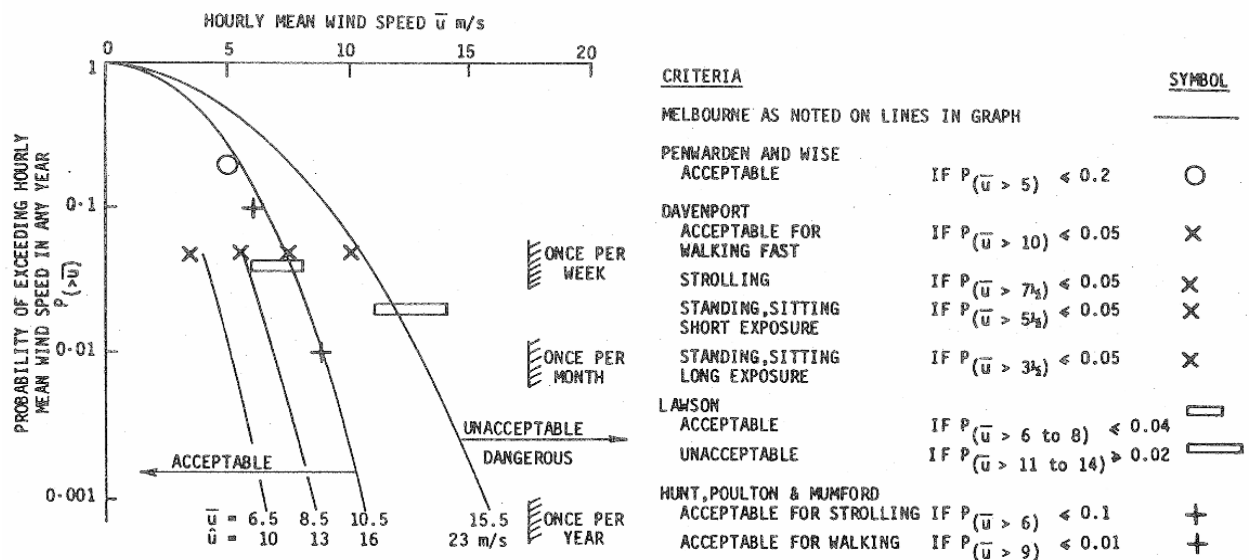


Figure A.1: Comparison of Various Mean and Gust Wind Environment Criteria, assuming 15% turbulence and a Gust Factor of 1.5 (W.H. Melbourne, 1978)

A.7 References relating to Pedestrian Comfort Criteria

Davenport, A.G., 1972, "An approach to human comfort criteria for environmental conditions". Colloquium on Building Climatology, Stockholm.

Davenport, A.G., 1977, "The prediction of risk under wind loading", 2nd International Conference on Structural Safety and Reliability, Munich, Germany, pp511-538.

Lawson, T.V., 1973, "The wind environment of buildings: a logical approach to the establishment of criteria". Bristol University, Department of Aeronautical Engineering.

Lawson, T.V., 1975, "The determination of the wind environment of a building complex before construction". Bristol University, Department of Aeronautical Engineering.

Melbourne, W.H., 1978, "Criteria for Environmental Wind Conditions". Journal of Wind Engineering and Industrial Aerodynamics, vol. 3, pp241-249.

Penwarden, A.D. (1973). "Acceptable Wind Speeds in Towns", Building Science, vol. 8: pp259-267.

Penwarden, A.D., Wise A.F.E., 1975, "Wind Environment Around Buildings". Building Research Establishment Report, London.

Rofail, A.W., 2007, "Comparison of Wind Environment Criteria against Field Observations". 12th International Conference of Wind Engineering, Cairns, Australia.

APPENDIX B DATA ACQUISITION

The wind tunnel testing procedures utilised for this study were based on the guidelines set out in the Australasian Wind Engineering Society Quality Assurance Manual (AWES-QAM-1-2019), ASCE 7-16 (Chapter C31), and CTBUH (2013). The wind speed measurements for the wind tunnel study were determined as coefficients using data acquired by either Dantec hot-wire probe anemometers or pressure-based wind speed sensors and converted to full-scale wind speeds using details of the regional wind climate obtained from an analysis of directional wind speed recordings from the local meteorological recording station(s).

B.1 Measurement of the Velocity Coefficients

The study model and proximity model were setup within the wind tunnel which was configured to the appropriate boundary layer profile, and the wind velocity measurements were monitored using either Dantec hot-wire probe anemometers or pressure-based wind speed sensors at selected critical outdoor locations. The wind velocity results presented in this study for each study point are representative of wind at a full-scale height of approximately 1.5m above ground/slab level. In the case of the Dantec hot-wire probe anemometers, the support of the probe is mounted such that the probe wire is vertical as much as possible to ensure that the measured wind speeds are independent of wind direction along the horizontal plane. In addition, care was taken in the alignment of the hot-wire probe wire and in avoiding wall-heating effects.

Wind speed measurements were made in the wind tunnel for 16 wind directions, at 22.5° increments. Data was acquired for each wind direction using a sample rate of 1024Hz. The sample length was determined to produce a full-scale sample time that is sufficient for this type of study. In the case of the pressure-based wind speed sensors, the phase lag between the various channels where data is acquired simultaneously is within 10% of a typical pressure cycle, and the signal is low-pass filtered at 500Hz and then digital filtering is applied over this range to provide an unbiased response from the pressure measurement system (A.W. Rofail, 2004).

The mean, gust and standard deviation velocity coefficients were determined from the data acquired in the wind tunnel. The gust velocity coefficients were also derived for each wind direction from by the following relation:

$$\hat{C}_V = \bar{C}_V + g \cdot \sigma_{C_V} \quad \text{B.1}$$

where:

\hat{C}_V is the gust velocity coefficient.

\bar{C}_V is the mean velocity coefficient.

g is the peak factor, taken as 3.0 for a 3-sec gust and 3.4 for a 0.5-sec gust.

σ_{C_V} is the standard deviation of the velocity coefficient measurement.

In the case of a Dantec hot-wire probe anemometer, the velocity coefficient is obtained as follows:

$$C_V = \frac{C_{V,study}}{C_{V,200m}} \quad B.2$$

where:

$C_{V,study}$ is the velocity coefficient measurement obtained from the Dantec hot-wire probe anemometer at the study point location.

$C_{V,200m}$ is the velocity coefficient measurement obtained from the Dantec hot-wire probe anemometer at the free-stream reference location at 200m height upwind of the model in the wind tunnel.

However, in the case of the pressure-based wind speed sensors, these are determined from the measured differential mean, standard deviation and maximum pressure coefficients obtained from the wind speed sensor. For this analysis all calculations are performed on the square root of the differential pressure measurements. The velocity coefficient at the pressure-based wind speed sensor location is then calculated as follows:

$$C_V = \frac{\alpha + \beta\sqrt{\Delta p}}{V_{200m}} \quad B.3$$

where:

C_V is the velocity coefficient measurement at the study point location.

α is a calibration coefficient for the pressure-based wind speed sensor.

β is a calibration coefficient for the pressure-based wind speed sensor.

Δp is the differential pressure obtained from the pressure-based wind speed sensor at the study point location.

V_{200m} is the wind speed at the free-stream reference location of 200m height (full-scale) in the wind tunnel, which is determined directly in the wind tunnel using a pitot static probe.

B.2 Calculation of the Full-Scale Results

The full-scale results determine if the wind conditions at a study location satisfy the designated criteria of that location. More specifically, the full-scale results need to determine the probability of exceedance of a given wind speed at a study location. To determine the probability of exceedance, the measured velocity coefficients were combined with a statistical model of the local wind climate that relates wind speed to a probability of exceedance. Details of the wind climate model are outlined in Section 4 of the main report.

The statistical model of the wind climate includes the impact of wind directionality as any local variations in wind speed or frequency with wind direction. This is important as the wind directions that produce the highest wind speed events for a region may not coincide with the most wind exposed direction at the site.

The methodology adopted for the derivation of the full-scale results for the maximum gust and the GEM wind speeds are outlined in the following sub-sections.

B.3 Maximum Gust Wind Speeds

The full-scale maximum gust wind speed at each study point location is derived from the velocity coefficient using the following relationship:

$$V_{study} = V_{ref,RH} \left(\frac{k_{200m,tr,T=1hr}}{k_{RH,tr,T=1hr}} \right) C_V \quad B.4$$

where:

V_{study} is the full-scale wind speed at the study point location.

$V_{ref,RH}$ is the full-scale reference wind speed at the study reference height. This value is determined by combining the directional wind speed data for the region (detailed in Section 4) and the upwind terrain and height multipliers for the site (detailed in Section 3).

$k_{200m,tr,T=1hr}$ is the hourly mean terrain and height multiplier at the free-stream reference location of 200m height.

$k_{RH,tr,T=1hr}$ is the hourly mean terrain and height multiplier at the study reference height (Section 3).

C_V is the velocity coefficient, obtained from either Equation B.2 (in the case of Dantec hot-wire probe anemometers) or Equation B.3 (in the case of pressure-based wind speed sensors).

The value of $V_{ref,RH}$ varies with each prevailing wind direction. Wind directions where there is a high probability that a strong wind will occur have a higher directional wind speed than other directions. To determine the directional wind speeds, a probability level must be assigned for each wind direction. These probability levels are set following the approach used in AS/NZS1170.2:2011, which assumes that the major contributions to the combined probability of exceedance of a typical load effect comes from only two 45 degree sectors.

B.4 Maximum Gust-Equivalent Mean Wind Speeds

The contribution to the probability of exceedance of a specified wind speed (ie: the desired wind speed for pedestrian comfort, as per the criteria) was calculated for each wind direction. These contributions are then combined over all wind directions to calculate the total probability of exceedance of the specified wind speed. To calculate the probability of exceedance for a specified wind speed a statistical wind climate model was used to describe the relationship between directional wind speeds and the probability of exceedance. A detailed description of the methodology is given by T.V. Lawson (1980).

The criteria used in this study is referenced to a probability of exceedance of 5% of a specified wind speed.

B.5 References relating to Data Acquisition

American Society of Civil Engineers (ASCE), ASCE-7-16, 2016, "Minimum Design Loads for Buildings and Other Structures".

Australasian Wind Engineering Society, QAM-1, 2019, "Quality Assurance Manual: Wind Engineering Studies of Buildings", edited by Rofail A.W., et al.

Council on Tall Buildings and Urban Habitat (CTBUH), 2013, "Wind tunnel testing of high-rise buildings", CTBUH Technical Guides.

Lawson, T.V., 1980, "Wind Effects on Buildings - Volume 1, Design Applications". Applied Science Publishers Ltd, Ripple Road, Barking, Essex, England.

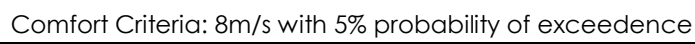
Rofail A.W., Tonin, R., and Hanafi, D., 2004, "Sensitivity of frequency response to type of tubing", Australasian Wind Engineering Workshop, Darwin.

Standards Australia and Standards New Zealand, AS/NZS 1170.2, 2011, "SAA Wind Loading Standard, Part 2: Wind Actions".



APPENDIX C DIRECTIONAL PLOTS OF WIND TUNNEL RESULTS

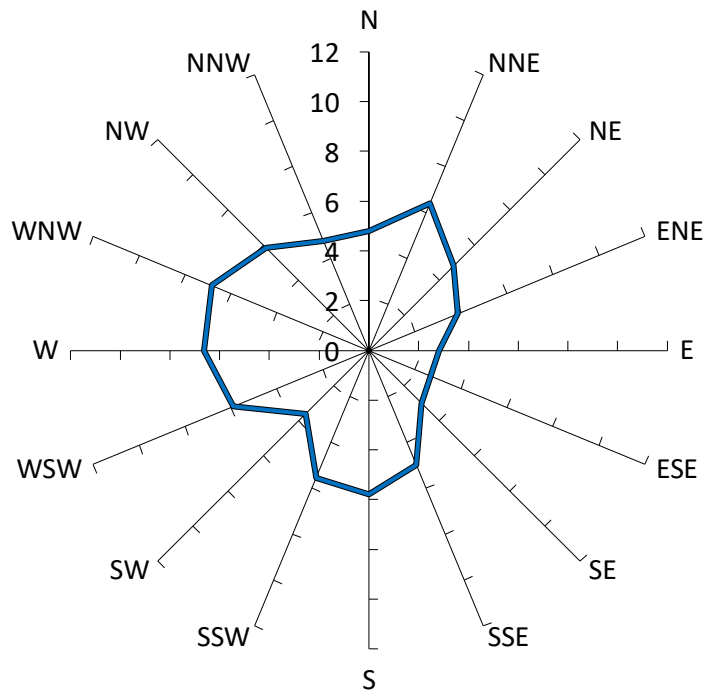
Gust Equivalent Mean (m/s)	Maximum Gust (m/s)
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WD758-22 Blackwattle Bay, Sydney June 1, 2022

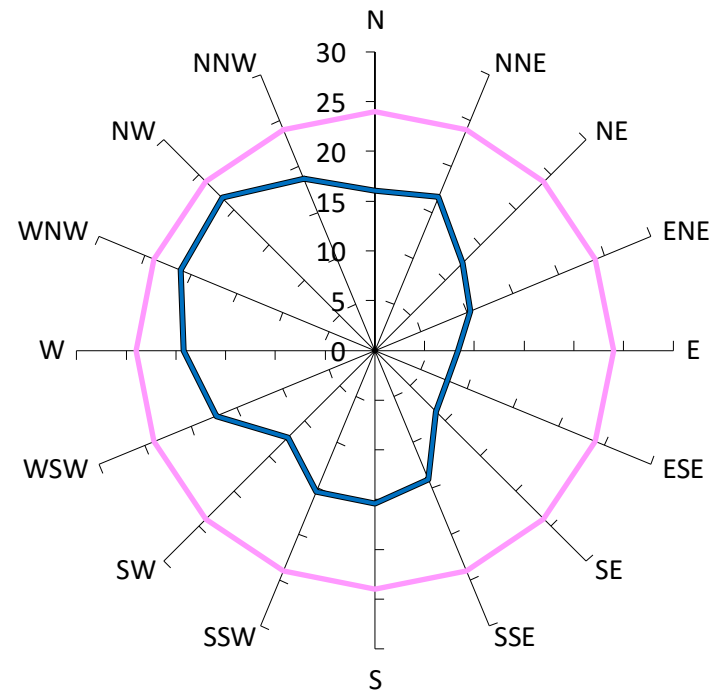
Results for P02

Gust Equivalent Mean (m/s)



Comfort Criteria: 8m/s with 5% probability of exceedence

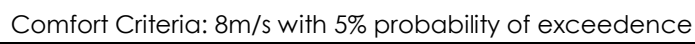
Maximum Gust (m/s)



Safety Limit: 24m/s

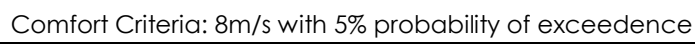
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Gust Equivalent Mean (m/s)	Maximum Gust (m/s)
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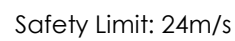
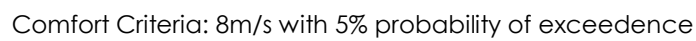
WD758-22 Blackwattle Bay, Sydney June 1, 2022

Gust Equivalent Mean (m/s)	Maximum Gust (m/s)
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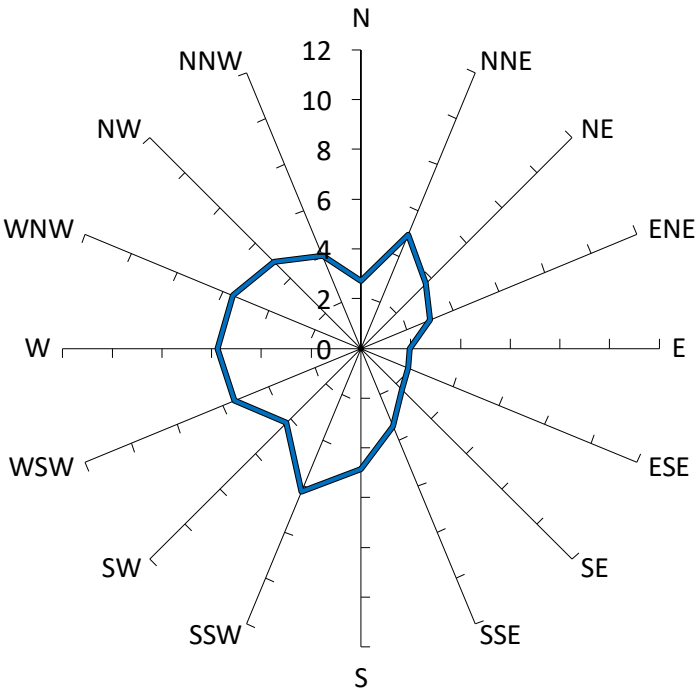
WD758-22 Blackwattle Bay, Sydney June 1, 2022

Gust Equivalent Mean (m/s)	Maximum Gust (m/s)
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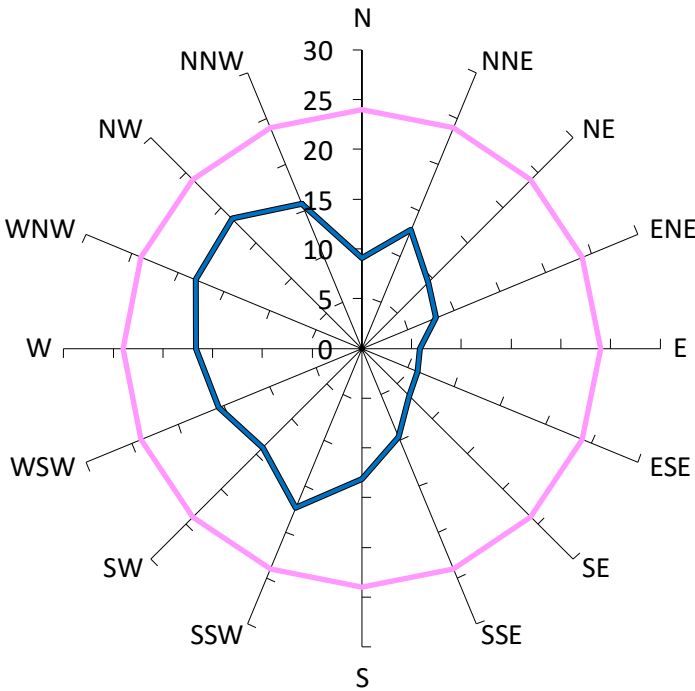
WD758-22 Blackwattle Bay, Sydney June 1, 2022

Results for P06

Gust Equivalent Mean (m/s)	Maximum Gust (m/s)
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Comfort Criteria: 8m/s with 5% probability of exceedence

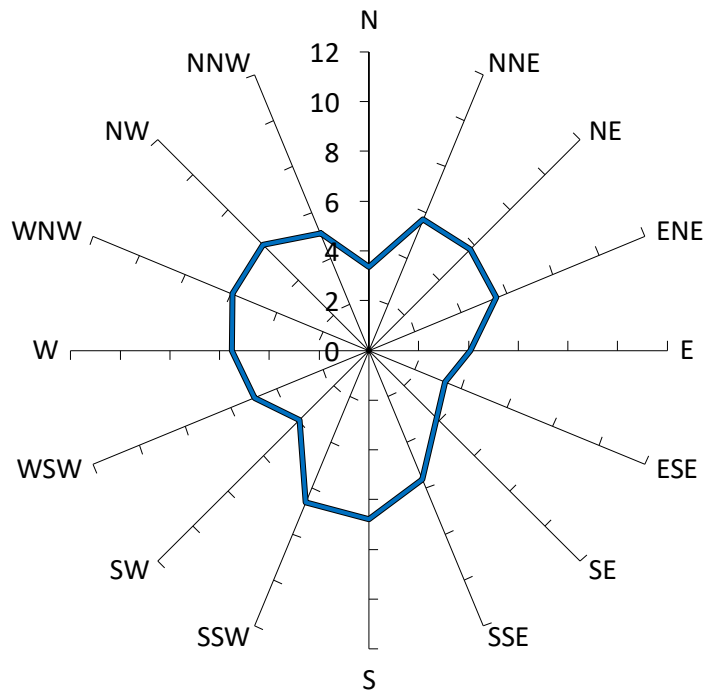


Safety Limit: 24m/s

Description	GEM Prob of Exceed %	Peak Gust m/s
<div></div> Criterion: Wind Comfort Standard for Walking Criterion (8m/s). Safety Limit (24m/s).	5%	24
<div></div> WD758-22 Proposed Massing Design and Awnings	1%	18
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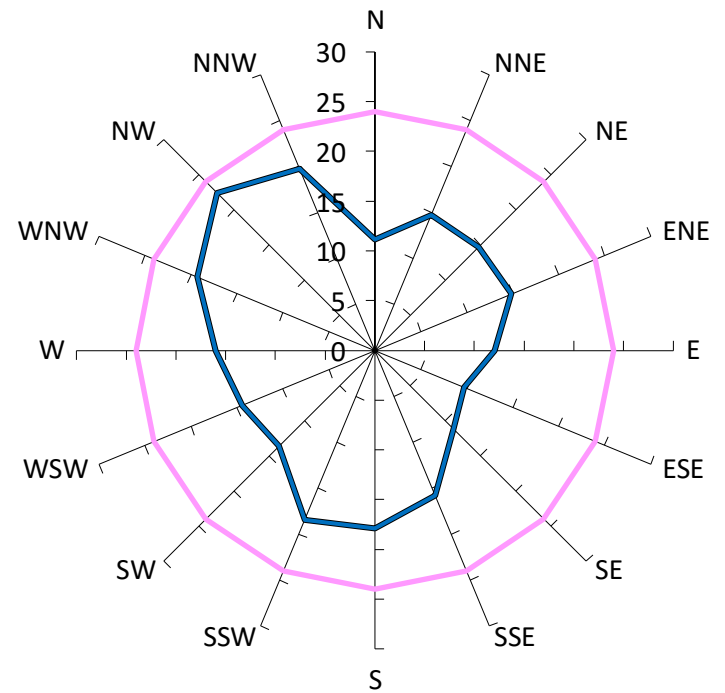
Results for P07

Gust Equivalent Mean (m/s)



Comfort Criteria: 8m/s with 5% probability of exceedence

Maximum Gust (m/s)

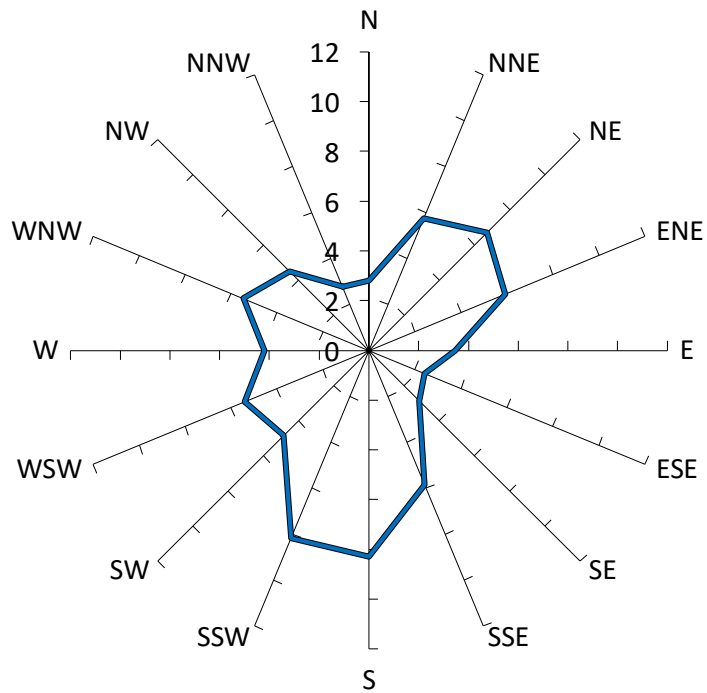


Safety Limit: 24m/s

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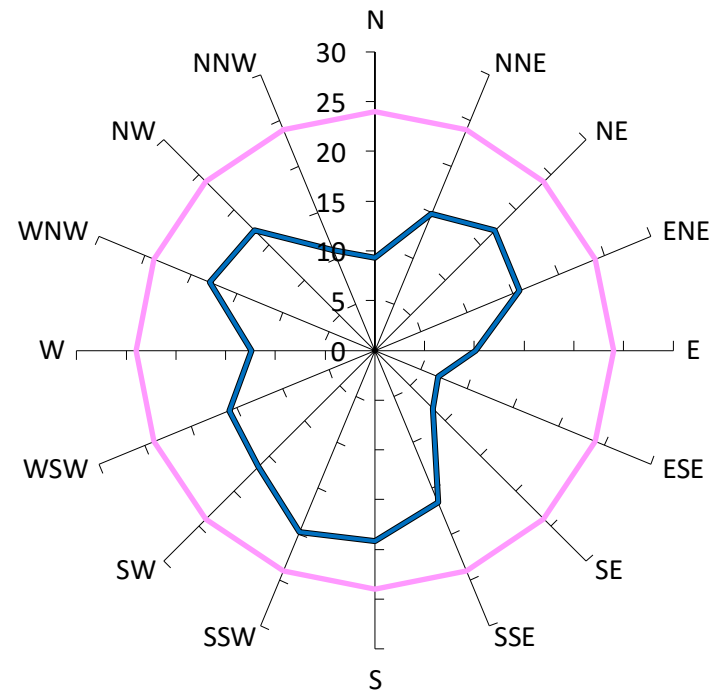
Results for P08

Gust Equivalent Mean (m/s)



Comfort Criteria: 8m/s with 5% probability of exceedence

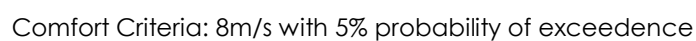
Maximum Gust (m/s)



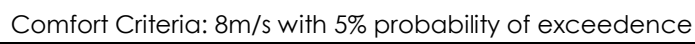
Safety Limit: 24m/s









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Gust Equivalent Mean (m/s)	Maximum Gust (m/s)
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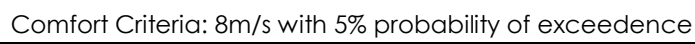
WD758-22 Blackwattle Bay, Sydney June 1, 2022

Gust Equivalent Mean (m/s)	Maximum Gust (m/s)
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Description		GEM Prob of Exceed %	Peak Gust m/s
	Criterion: Wind Comfort Standard for Walking Criterion (8m/s). Safety Limit (24m/s).	5%	24
	WD758-22 Proposed Massing Design and Awnings	3%	23
			
			
			
			
			
			

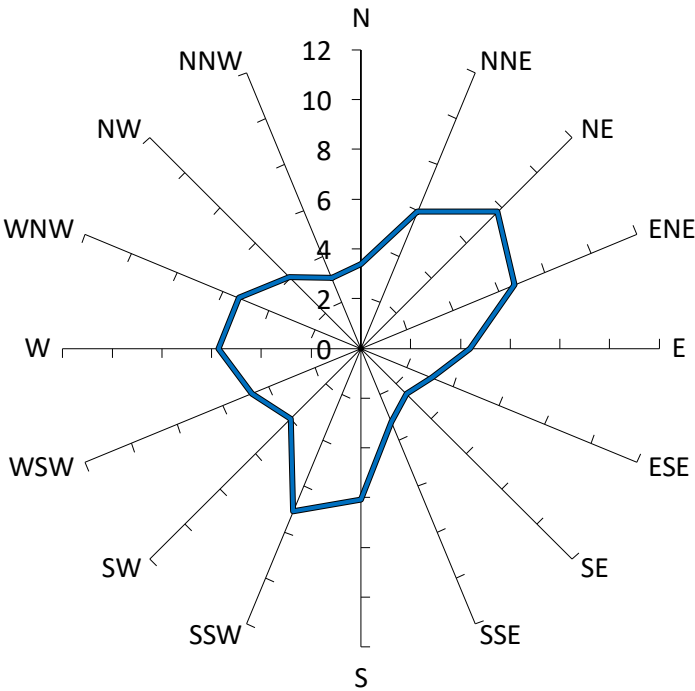
Gust Equivalent Mean (m/s)	Maximum Gust (m/s)
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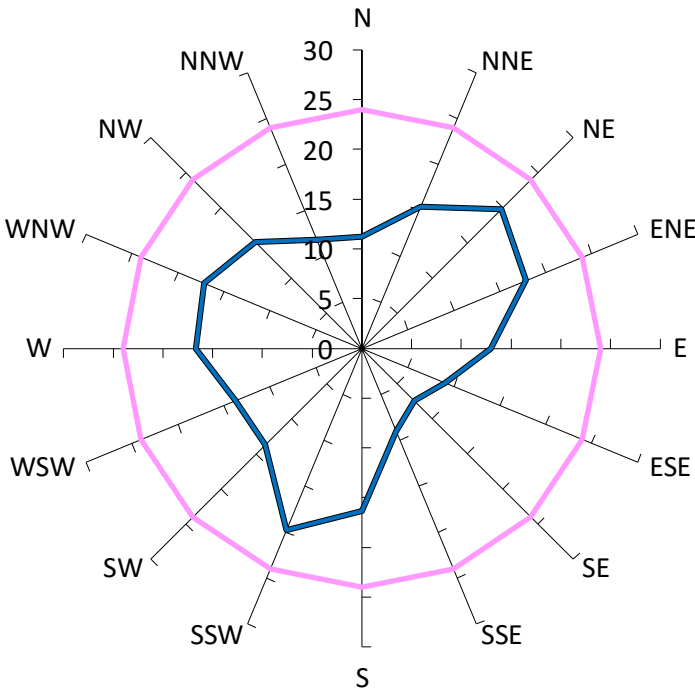
WD758-22 Blackwattle Bay, Sydney June 1, 2022

Results for P12

Gust Equivalent Mean (m/s)	Maximum Gust (m/s)
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Comfort Criteria: 8m/s with 5% probability of exceedence

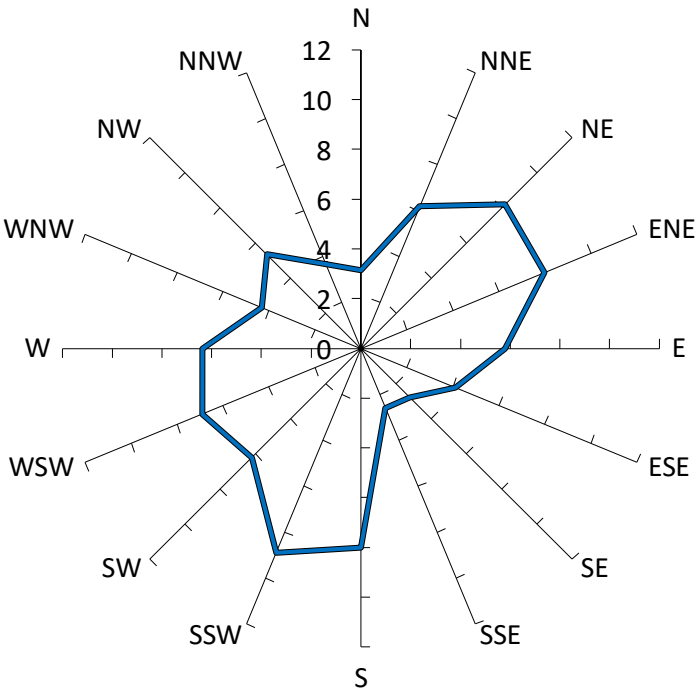


Safety Limit: 24m/s

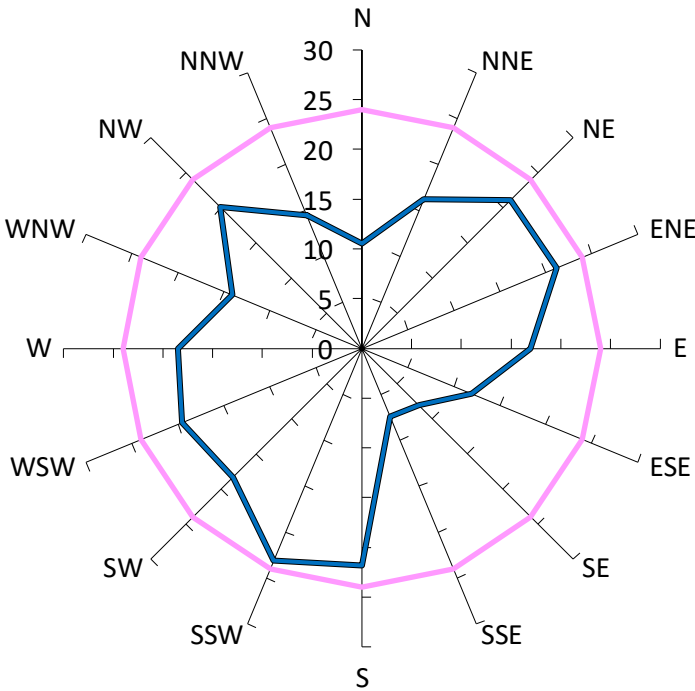
Description	GEM Prob of Exceed %	Peak Gust m/s
<div></div> Criterion: Wind Comfort Standard for Walking Criterion (8m/s). Safety Limit (24m/s).	5%	24
<div></div> WD758-22 Proposed Massing Design and Awnings	2%	20
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Results for P13

Gust Equivalent Mean (m/s)	Maximum Gust (m/s)
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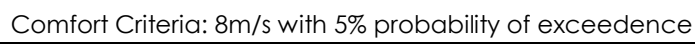
Comfort Criteria: 8m/s with 5% probability of exceedence



Safety Limit: 24m/s

Description	GEM Prob of Exceed %	Peak Gust m/s
<div></div> Criterion: Wind Comfort Standard for Walking Criterion (8m/s). Safety Limit (24m/s).	5%	24
<div></div> WD758-22 Proposed Massing Design and Awnings	7%	23
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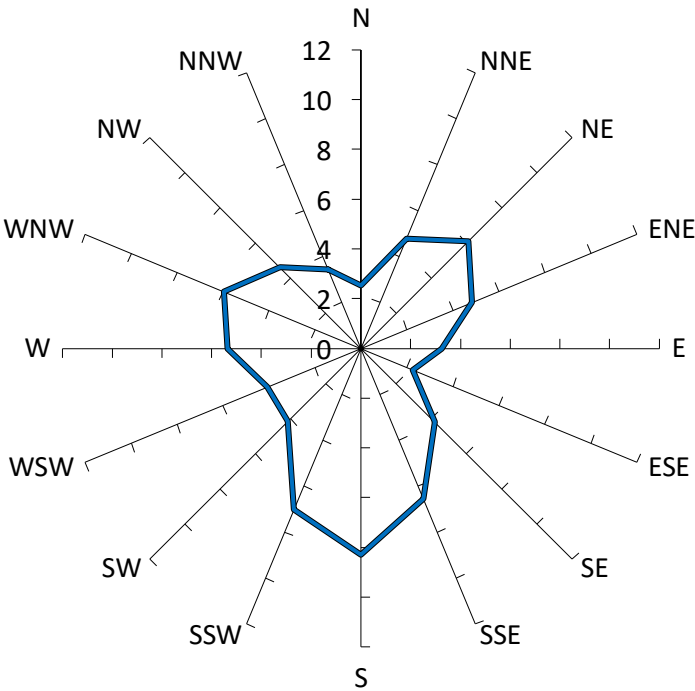
Gust Equivalent Mean (m/s)	Maximum Gust (m/s)
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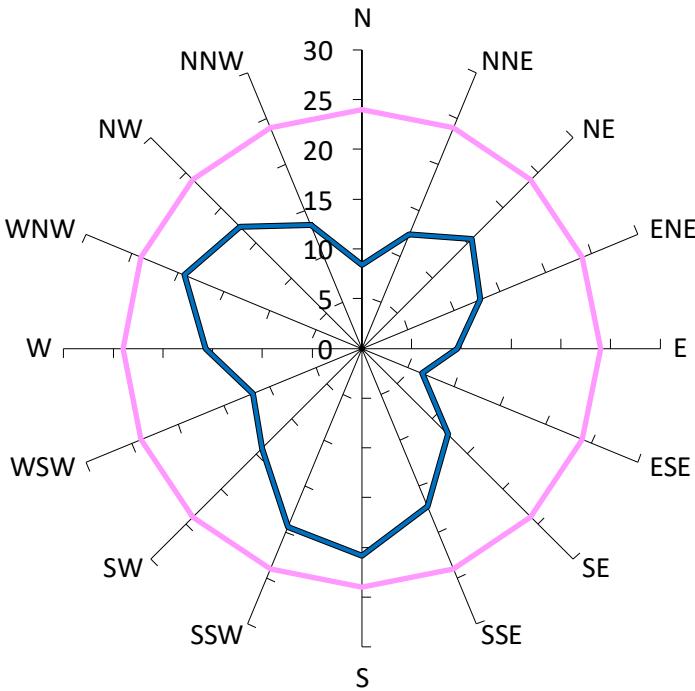
WD758-22 Blackwattle Bay, Sydney June 1, 2022

Results for P15

Gust Equivalent Mean (m/s)	Maximum Gust (m/s)
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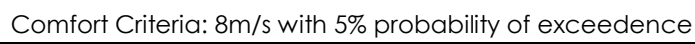
Comfort Criteria: 8m/s with 5% probability of exceedence



Safety Limit: 24m/s

Description	GEM Prob of Exceed %	Peak Gust m/s
<div></div> Criterion: Wind Comfort Standard for Walking Criterion (8m/s). Safety Limit (24m/s).	5%	24
<div></div> WD758-22 Proposed Massing Design and Awnings	3%	21
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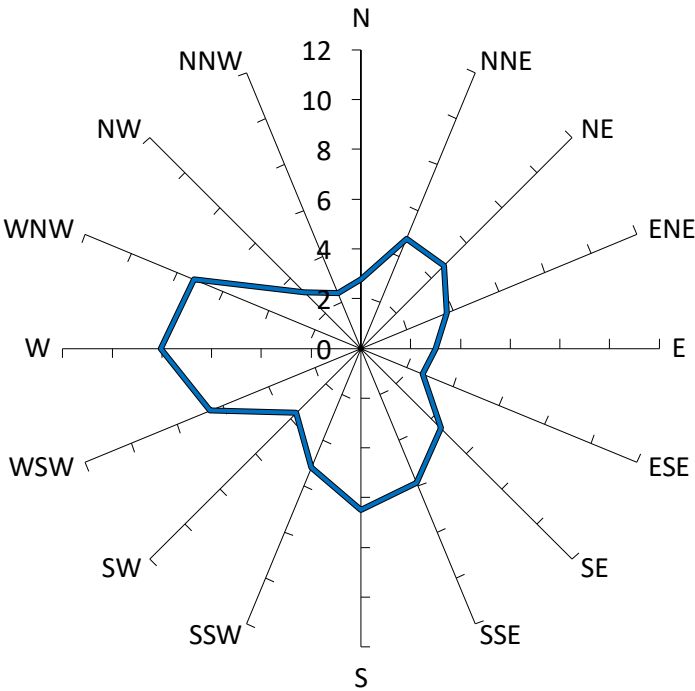
Gust Equivalent Mean (m/s)	Maximum Gust (m/s)
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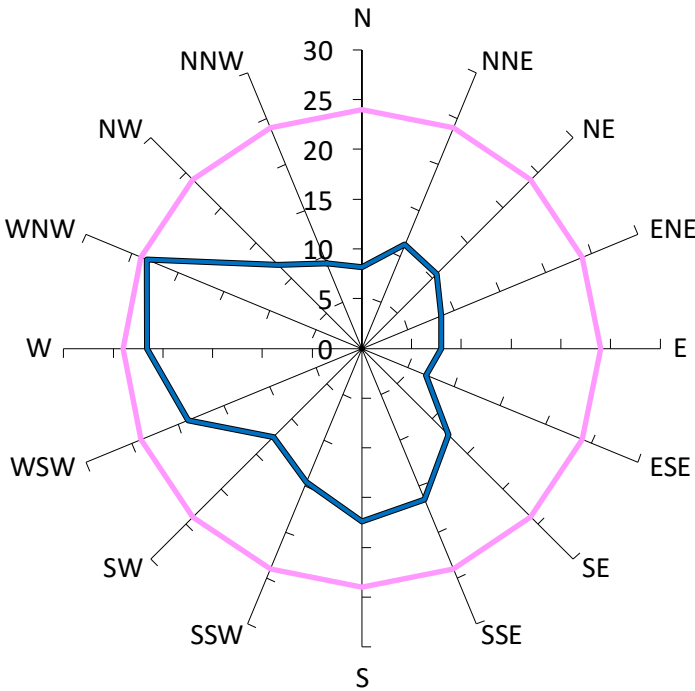
WD758-22 Blackwattle Bay, Sydney June 1, 2022

Results for P17

Gust Equivalent Mean (m/s)	Maximum Gust (m/s)
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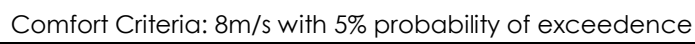
Comfort Criteria: 8m/s with 5% probability of exceedence



Safety Limit: 24m/s

Description	GEM Prob of Exceed %	Peak Gust m/s
<div></div> Criterion: Wind Comfort Standard for Walking Criterion (8m/s). Safety Limit (24m/s).	5%	24
<div></div> WD758-22 Proposed Massing Design and Awnings	3%	23
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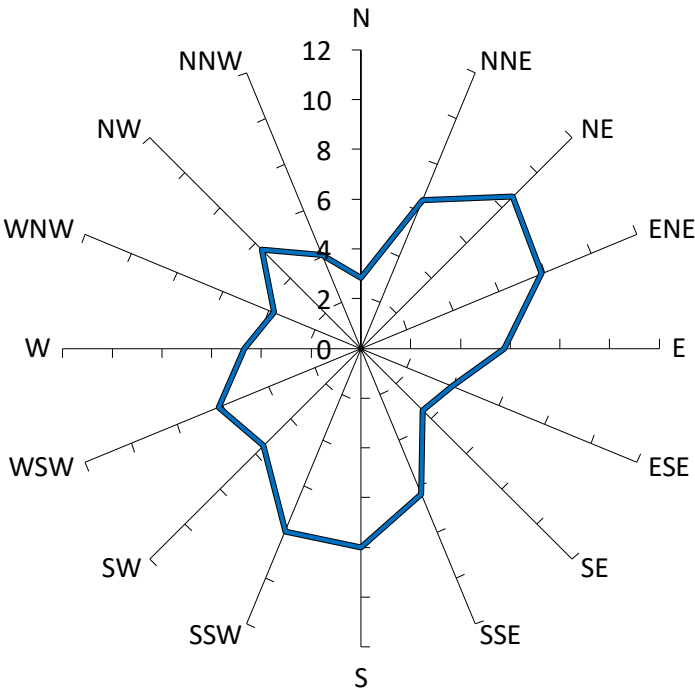
Gust Equivalent Mean (m/s)	Maximum Gust (m/s)
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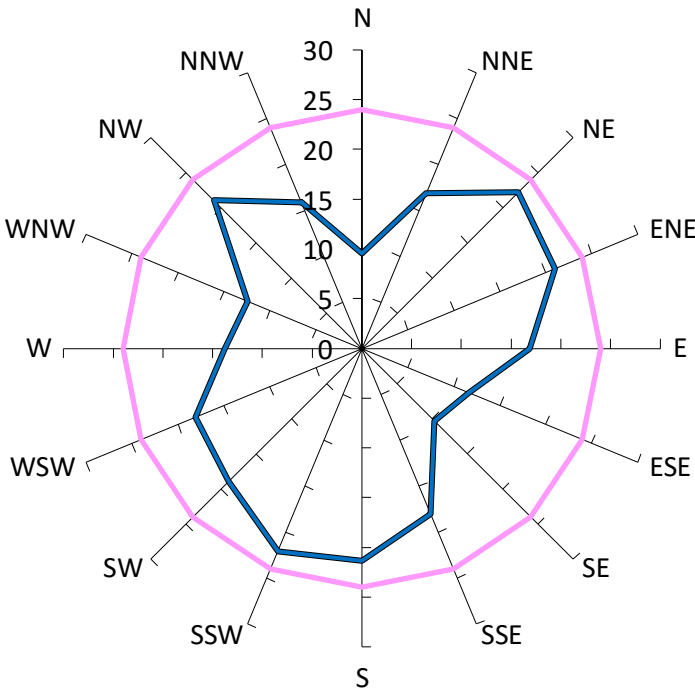
WD758-22 Blackwattle Bay, Sydney June 1, 2022

Results for P19

Gust Equivalent Mean (m/s)	Maximum Gust (m/s)
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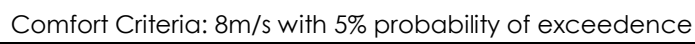
Comfort Criteria: 8m/s with 5% probability of exceedence



Safety Limit: 24m/s

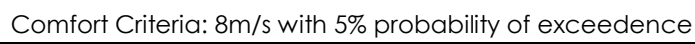
Description	GEM Prob of Exceed %	Peak Gust m/s
<div></div> Criterion: Wind Comfort Standard for Walking Criterion (8m/s). Safety Limit (24m/s).	5%	24
<div></div> WD758-22 Proposed Massing Design and Awnings	7%	22
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Gust Equivalent Mean (m/s)	Maximum Gust (m/s)
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WD758-22 Blackwattle Bay, Sydney June 1, 2022

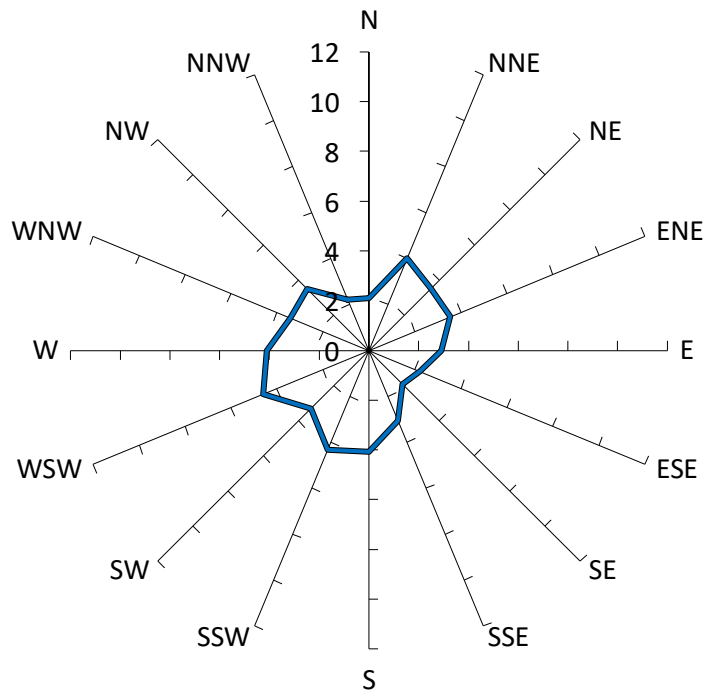
Gust Equivalent Mean (m/s)	Maximum Gust (m/s)
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Description		GEM Prob of Exceed %	Peak Gust m/s
	Criterion: Wind Comfort Standard for Walking Criterion (8m/s). Safety Limit (24m/s).	5%	24
	WD758-22 Proposed Massing Design and Awnings	< 1%	16
			
			
			
			
			
			

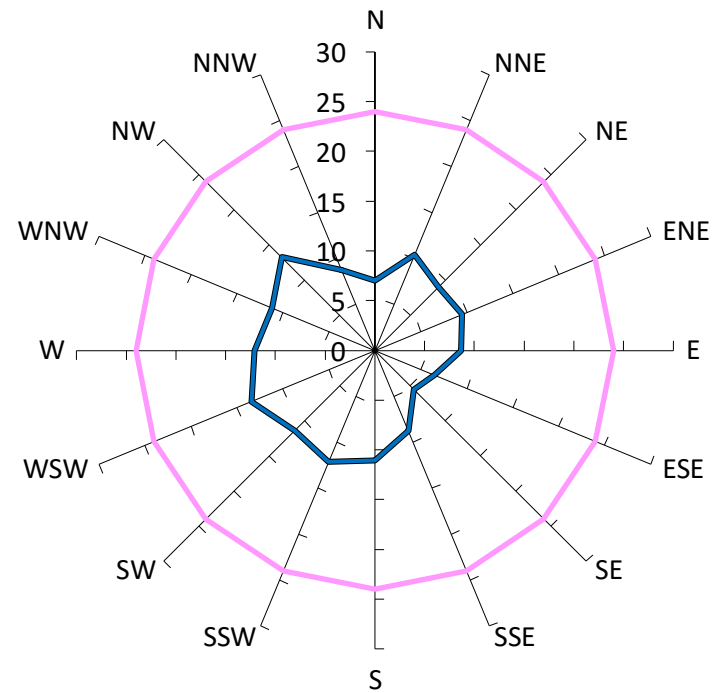
Results for P22

Gust Equivalent Mean (m/s)








Comfort Criteria: 8m/s with 5% probability of exceedence

Maximum Gust (m/s)

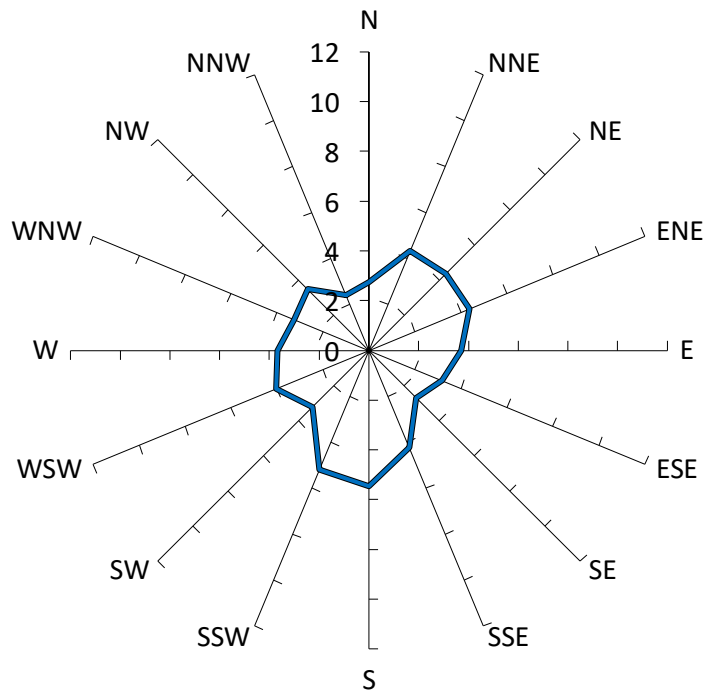


Safety Limit: 24m/s

Description		GEM Prob of Exceed %	Peak Gust m/s
	Criterion: Wind Comfort Standard for Walking Criterion (8m/s). Safety Limit (24m/s).	5%	24
	WD758-22 Proposed Massing Design and Awnings	< 1%	13
			
			
			
			
			
			
			

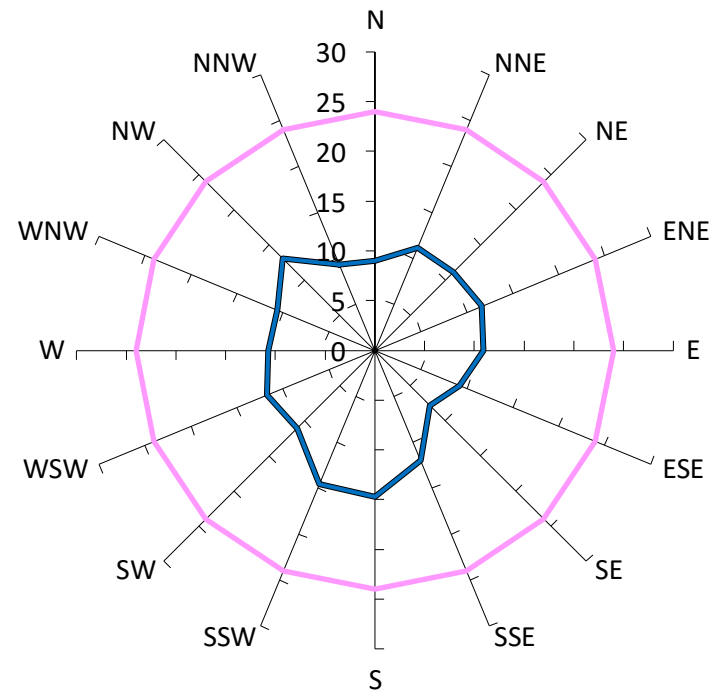
Results for P23

Gust Equivalent Mean (m/s)



Comfort Criteria: 8m/s with 5% probability of exceedence

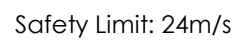
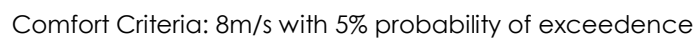
Maximum Gust (m/s)



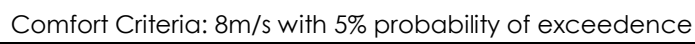
Safety Limit: 24m/s









[illegible]

Gust Equivalent Mean (m/s)	Maximum Gust (m/s)
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WD758-22 Blackwattle Bay, Sydney June 1, 2022

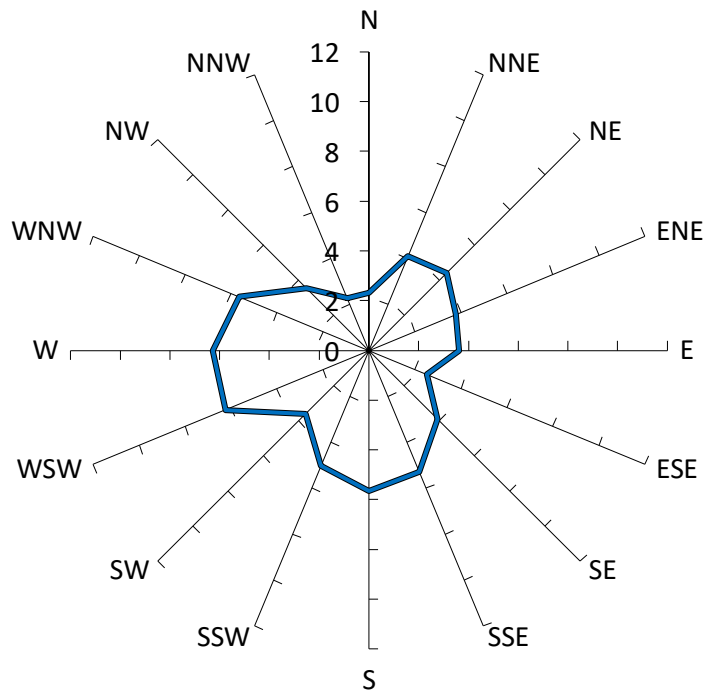
Gust Equivalent Mean (m/s)	Maximum Gust (m/s)
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Description		GEM Prob of Exceed %	Peak Gust m/s
	Criterion: Wind Comfort Standard for Walking Criterion (8m/s). Safety Limit (24m/s).	5%	24
	WD758-22 Proposed Massing Design and Awnings	4%	19
			
			
			
			
			
			

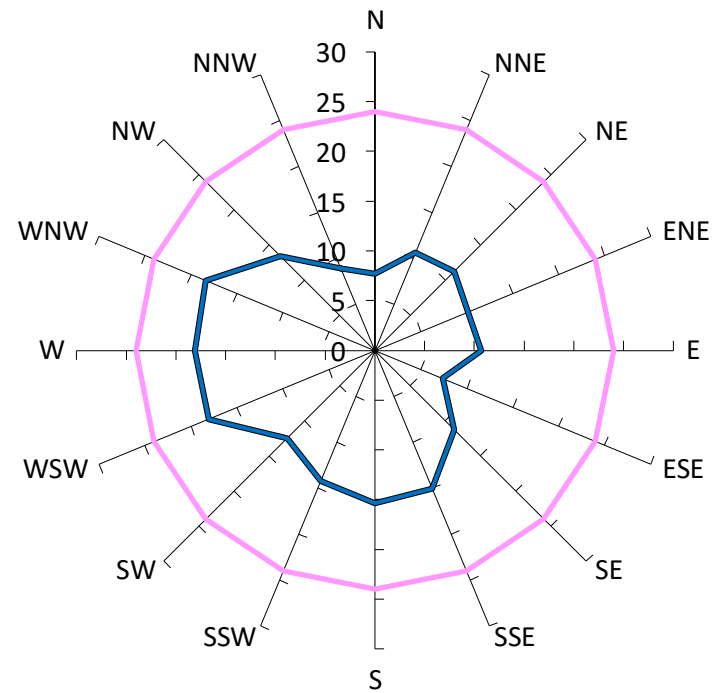
Results for P26

Gust Equivalent Mean (m/s)



Comfort Criteria: 8m/s with 5% probability of exceedence

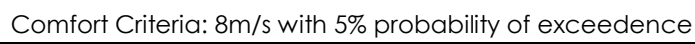
Maximum Gust (m/s)



Safety Limit: 24m/s

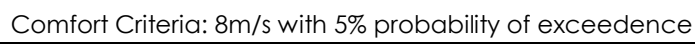
[illegible]

Gust Equivalent Mean (m/s)	Maximum Gust (m/s)
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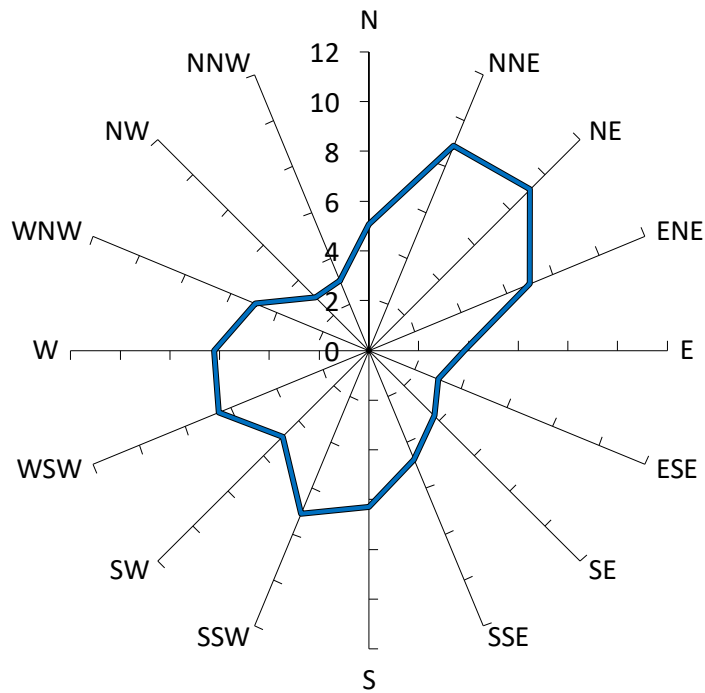
WD758-22 Blackwattle Bay, Sydney June 1, 2022

Gust Equivalent Mean (m/s)	Maximum Gust (m/s)
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[illegible]

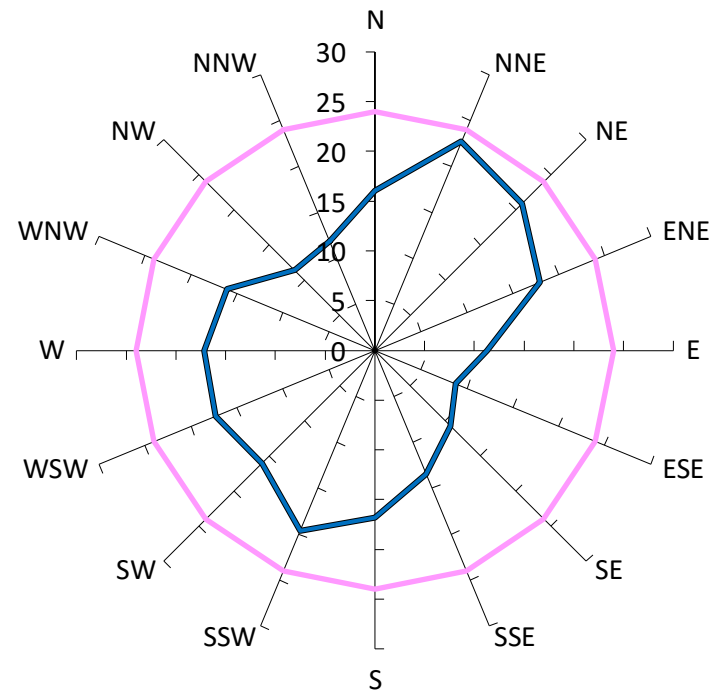
Results for P29

Gust Equivalent Mean (m/s)



Comfort Criteria: 8m/s with 5% probability of exceedence

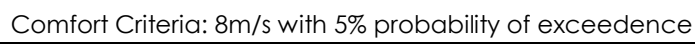
Maximum Gust (m/s)











Safety Limit: 24m/s

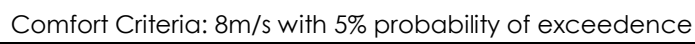
[illegible]

Gust Equivalent Mean (m/s)	Maximum Gust (m/s)
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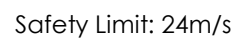
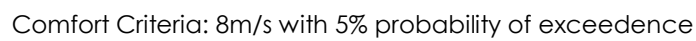
Description		GEM Prob of Exceed %	Peak Gust m/s
	Criterion: Wind Comfort Standard for Walking Criterion (8m/s). Safety Limit (24m/s).	5%	24
	WD758-22 Proposed Massing Design and Awnings	15%	24
			
			
			
			
			
			

Gust Equivalent Mean (m/s)	Maximum Gust (m/s)
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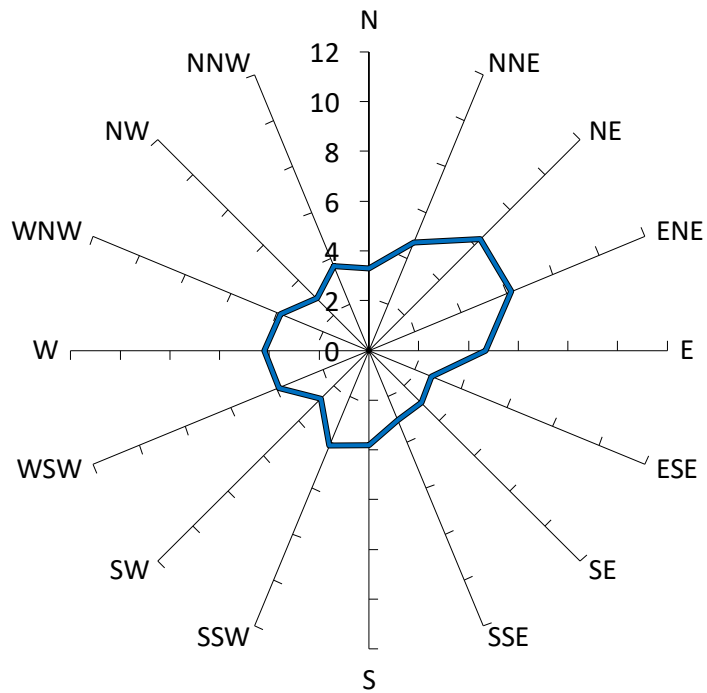
WD758-22 Blackwattle Bay, Sydney June 1, 2022

Gust Equivalent Mean (m/s)	Maximum Gust (m/s)
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WD758-22 Blackwattle Bay, Sydney June 1, 2022

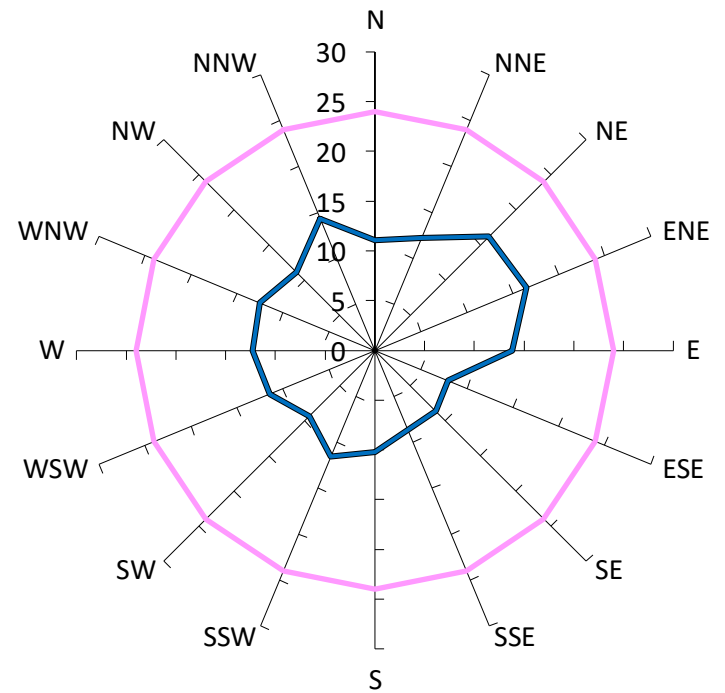
Results for P33

Gust Equivalent Mean (m/s)






Comfort Criteria: 8m/s with 5% probability of exceedence

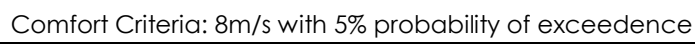
Maximum Gust (m/s)










Safety Limit: 24m/s

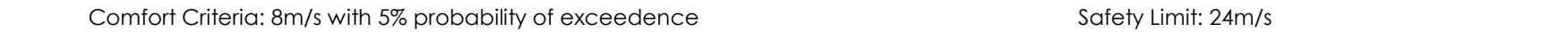
Description		GEM Prob of Exceed %	Peak Gust m/s
	Criterion: Wind Comfort Standard for Walking Criterion (8m/s). Safety Limit (24m/s).	5%	24
	WD758-22 Proposed Massing Design and Awnings	< 1%	16
			
			
			
			
			
			









Gust Equivalent Mean (m/s)	Maximum Gust (m/s)
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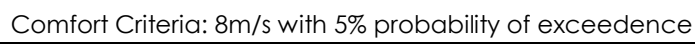
	Description	GEM Prob of Exceed %	Peak Gust m/s
	Criterion: Wind Comfort Standard for Walking Criterion (8m/s). Safety Limit (24m/s).	5%	24
	WD758-22 Proposed Massing Design and Awnings	7%	24
			
			
			
			
			
			
			

Gust Equivalent Mean (m/s)	Maximum Gust (m/s)
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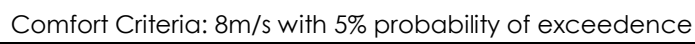
Description		GEM Prob of Exceed %	Peak Gust m/s
	Criterion: Wind Comfort Standard for Walking Criterion (8m/s). Safety Limit (24m/s).	5%	24
	WD758-22 Proposed Massing Design and Awnings	1%	21
			
			
			
			
			
			









Gust Equivalent Mean (m/s)	Maximum Gust (m/s)
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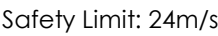
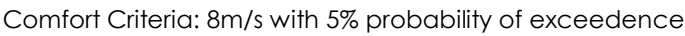
WD758-22 Blackwattle Bay, Sydney June 1, 2022




Gust Equivalent Mean (m/s)	Maximum Gust (m/s)
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	Description	GEM Prob of Exceed %	Peak Gust m/s
	Criterion: Wind Comfort Standard for Walking Criterion (8m/s). Safety Limit (24m/s).	5%	24
	WD758-22 Proposed Massing Design and Awnings	5%	22
			
			
			
			
			
			

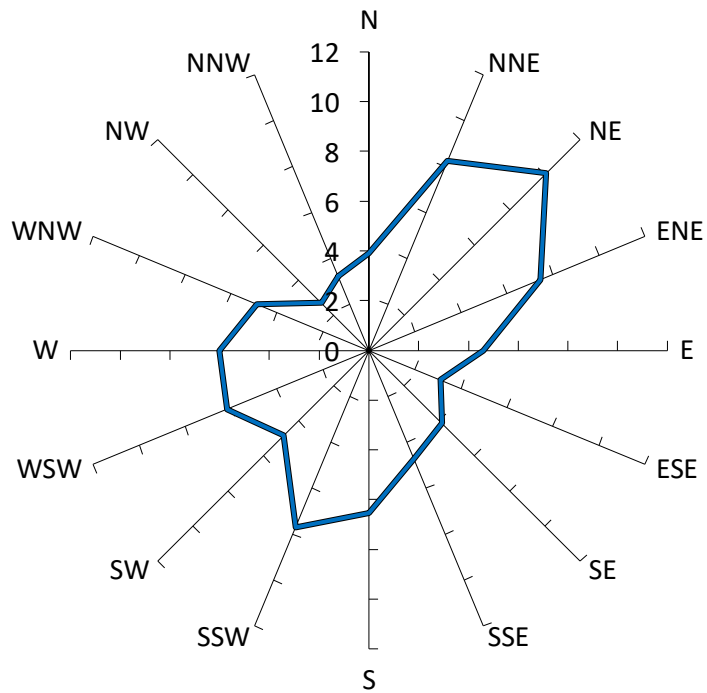
Gust Equivalent Mean (m/s)	Maximum Gust (m/s)
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Description		GEM Prob of Exceed %	Peak Gust m/s
	Criterion: Wind Comfort Standard for Walking Criterion (8m/s). Safety Limit (24m/s).	5%	24
	WD758-22 Proposed Massing Design and Awnings	8%	23
			
			
			
			
			
			
			

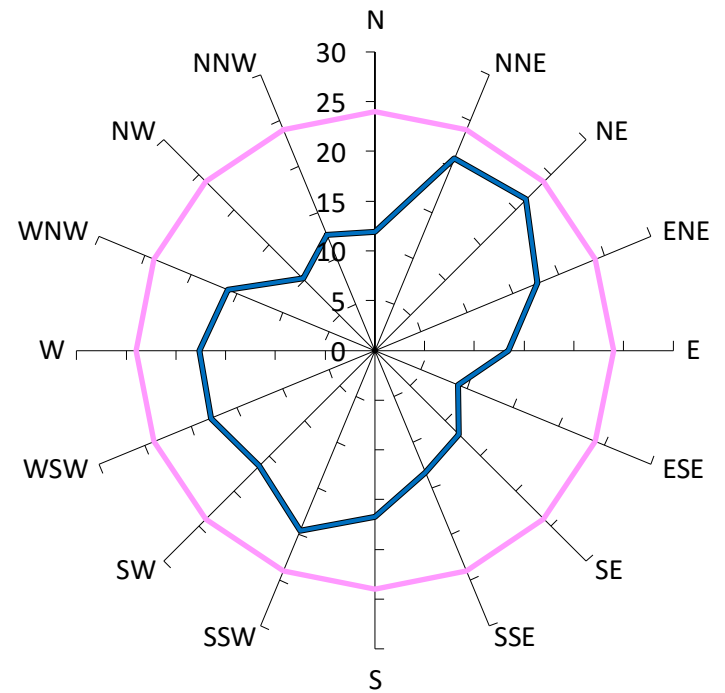
Results for P39

Gust Equivalent Mean (m/s)



Comfort Criteria: 8m/s with 5% probability of exceedence

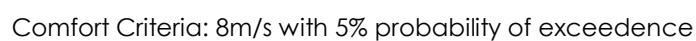
Maximum Gust (m/s)



Safety Limit: 24m/s

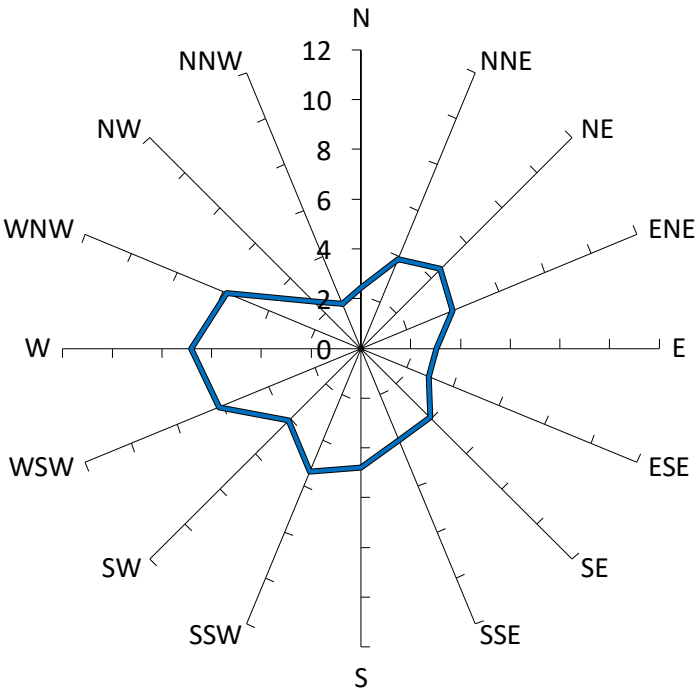
[illegible]

Gust Equivalent Mean (m/s)	Maximum Gust (m/s)
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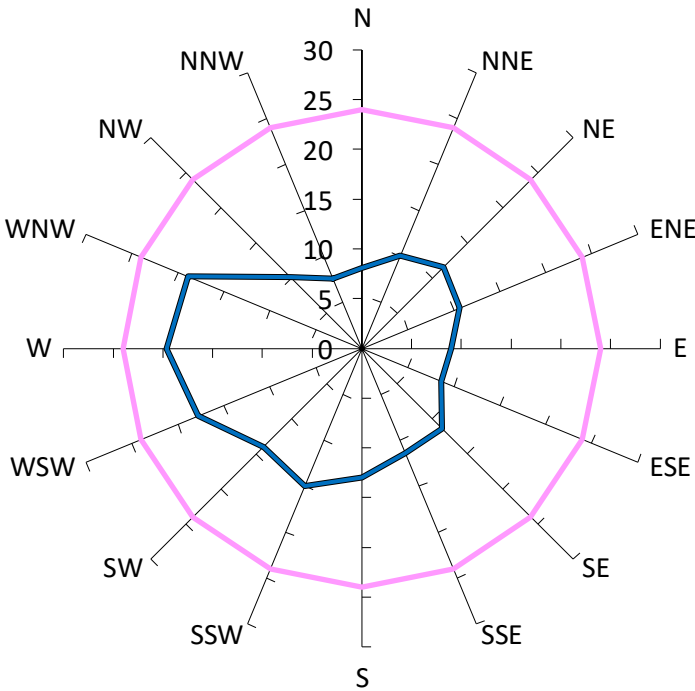
WD758-22 Blackwattle Bay, Sydney June 1, 2022

Results for P41

Gust Equivalent Mean (m/s)	Maximum Gust (m/s)
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Comfort Criteria: 8m/s with 5% probability of exceedence

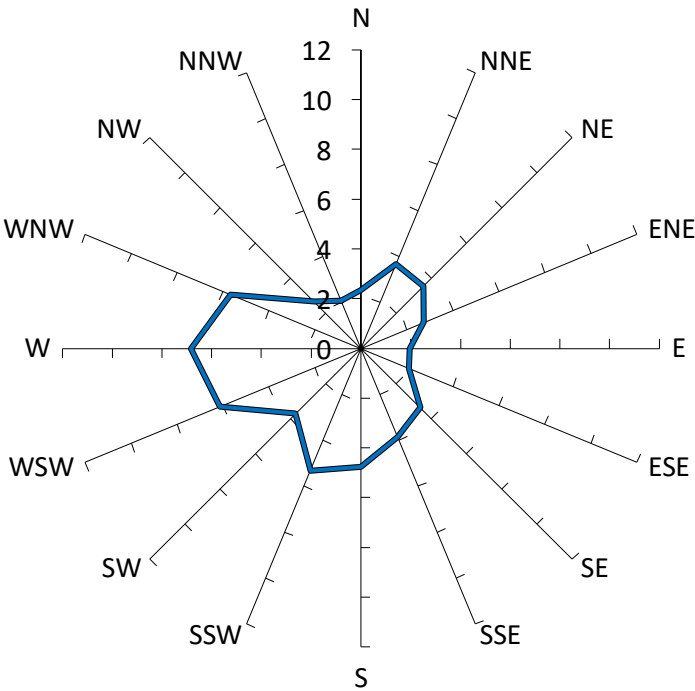


Safety Limit: 24m/s

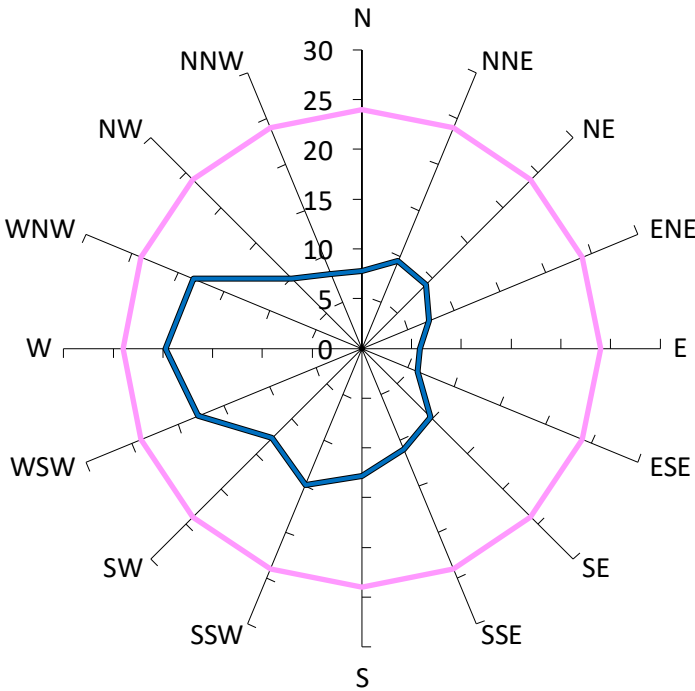
Description	GEM Prob of Exceed %	Peak Gust m/s
<div></div> Criterion: Wind Comfort Standard for Walking Criterion (8m/s). Safety Limit (24m/s).	5%	24
<div></div> WD758-22 Proposed Massing Design and Awnings	1%	20
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Results for P42

Gust Equivalent Mean (m/s)	Maximum Gust (m/s)
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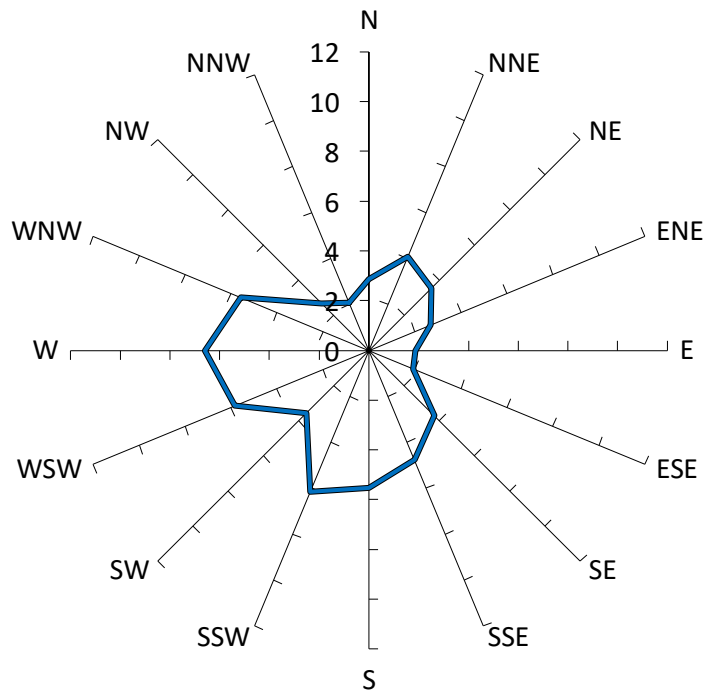
Comfort Criteria: 8m/s with 5% probability of exceedence



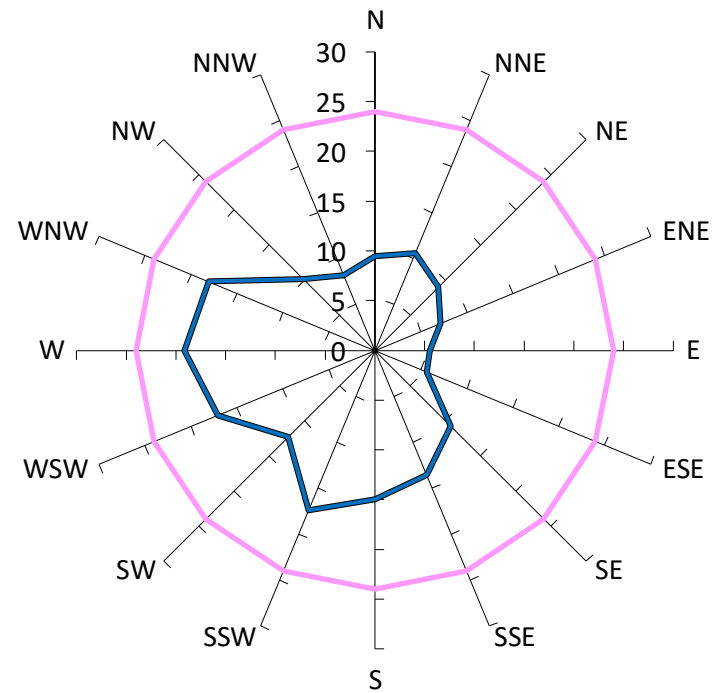
Safety Limit: 24m/s

Description	GEM Prob of Exceed %	Peak Gust m/s
<div></div> Criterion: Wind Comfort Standard for Walking Criterion (8m/s). Safety Limit (24m/s).	5%	24
<div></div> WD758-22 Proposed Massing Design and Awnings	1%	20
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Results for P43



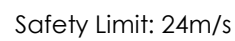
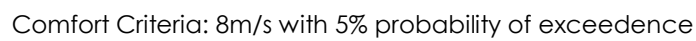
Comfort Criteria: 8m/s with 5% probability of exceedence



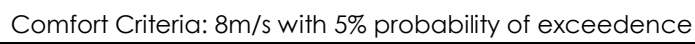
Safety Limit: 24m/s

Description		GEM Prob of Exceed %	Peak Gust m/s
	Criterion: Wind Comfort Standard for Walking Criterion (8m/s). Safety Limit (24m/s).	5%	24
	WD758-22 Proposed Massing Design and Awnings	1%	19
			
			
			
			
			
			
			

Gust Equivalent Mean (m/s)	Maximum Gust (m/s)
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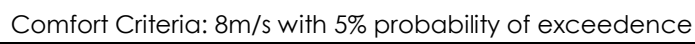
WD758-22 Blackwattle Bay, Sydney June 1, 2022










Gust Equivalent Mean (m/s)	Maximum Gust (m/s)
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WD758-22 Blackwattle Bay, Sydney June 1, 2022

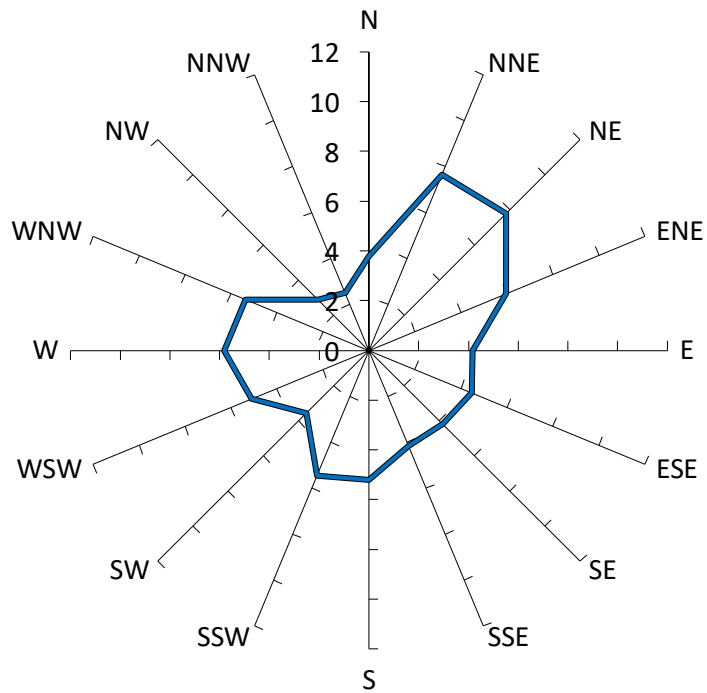
Gust Equivalent Mean (m/s)	Maximum Gust (m/s)
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Description		GEM Prob of Exceed %	Peak Gust m/s
	Criterion: Wind Comfort Standard for Walking Criterion (8m/s). Safety Limit (24m/s).	5%	24
	WD758-22 Proposed Massing Design and Awnings	4%	22
			
			
			
			
			
			
			

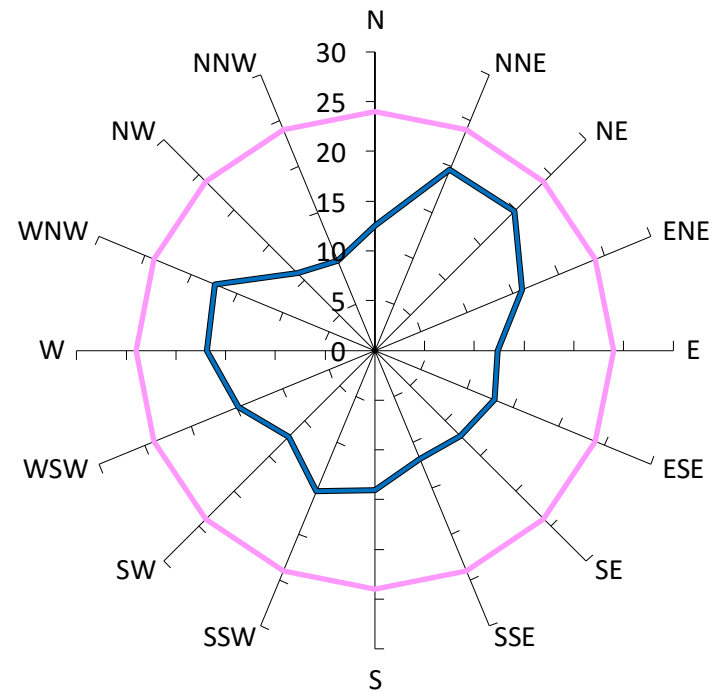
Results for P47

Gust Equivalent Mean (m/s)








Comfort Criteria: 8m/s with 5% probability of exceedence

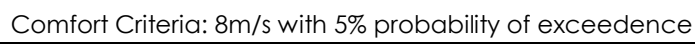
Maximum Gust (m/s)



Safety Limit: 24m/s

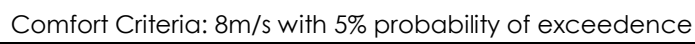
Description		GEM Prob of Exceed %	Peak Gust m/s
	Criterion: Wind Comfort Standard for Walking Criterion (8m/s). Safety Limit (24m/s).	5%	24
	WD758-22 Proposed Massing Design and Awnings	2%	20
			
			
			
			
			
			
			

Gust Equivalent Mean (m/s)	Maximum Gust (m/s)
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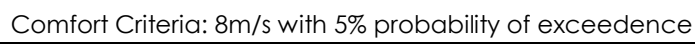
WD758-22 Blackwattle Bay, Sydney June 1, 2022







Gust Equivalent Mean (m/s)	Maximum Gust (m/s)
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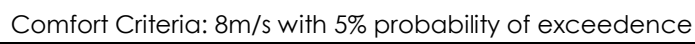
WD758-22 Blackwattle Bay, Sydney June 1, 2022

Gust Equivalent Mean (m/s)	Maximum Gust (m/s)
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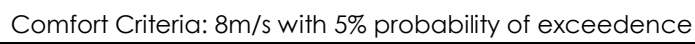
Description		GEM Prob of Exceed %	Peak Gust m/s
	Criterion: Wind Comfort Standard for Walking Criterion (8m/s). Safety Limit (24m/s).	5%	24
	WD758-22 Proposed Massing Design and Awnings	7%	21
			
			
			
			
			
			

Gust Equivalent Mean (m/s)	Maximum Gust (m/s)
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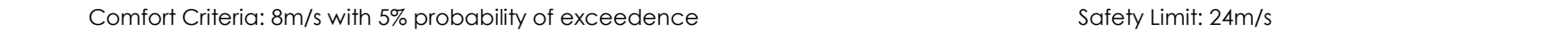
WD758-22 Blackwattle Bay, Sydney June 1, 2022

Gust Equivalent Mean (m/s)	Maximum Gust (m/s)
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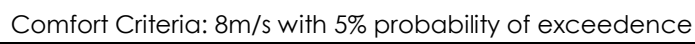


WD758-22 Blackwattle Bay, Sydney June 1, 2022

Gust Equivalent Mean (m/s)	Maximum Gust (m/s)
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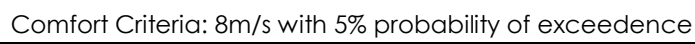
[illegible]





Gust Equivalent Mean (m/s)	Maximum Gust (m/s)
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WD758-22 Blackwattle Bay, Sydney June 1, 2022

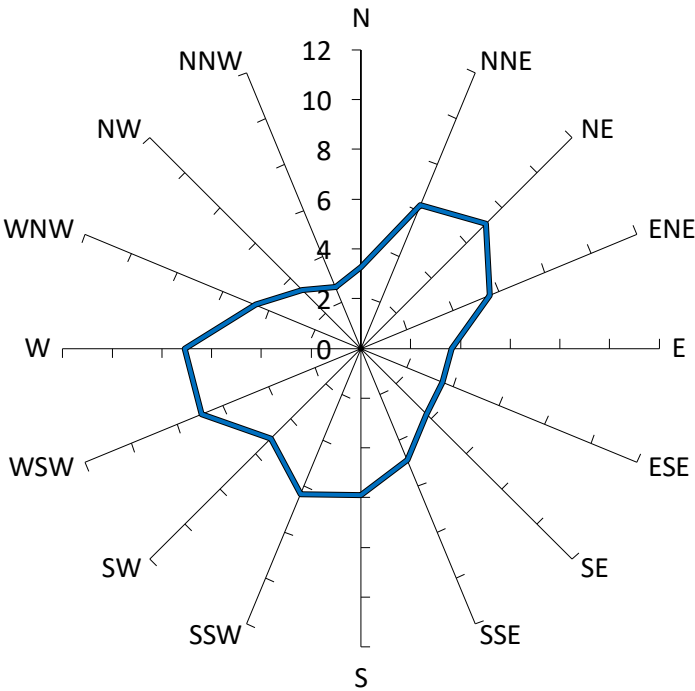
Gust Equivalent Mean (m/s)	Maximum Gust (m/s)
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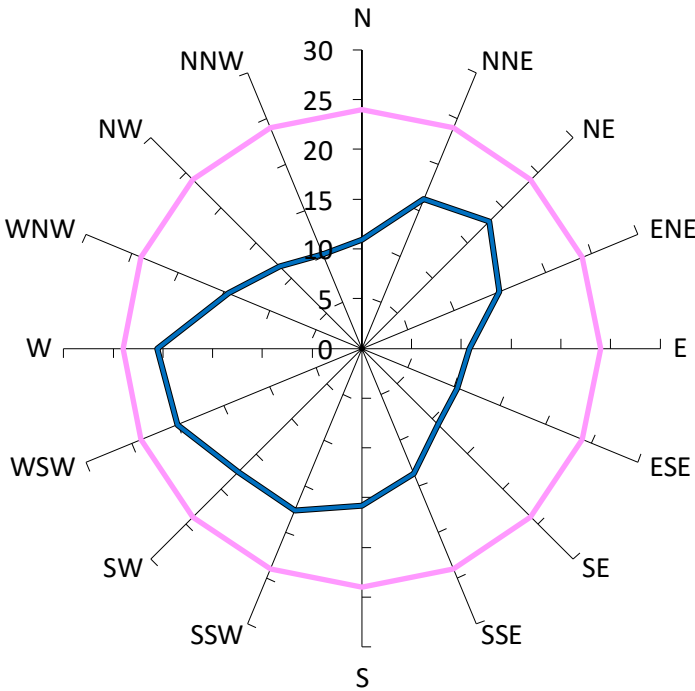
	Description	GEM Prob of Exceed %	Peak Gust m/s
	Criterion: Wind Comfort Standard for Walking Criterion (8m/s). Safety Limit (24m/s).	5%	24
	WD758-22 Proposed Massing Design and Awnings	15%	24
			
			
			
			
			
			

Results for P56

Gust Equivalent Mean (m/s)	Maximum Gust (m/s)
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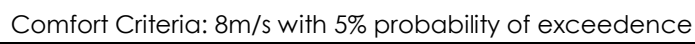
Comfort Criteria: 8m/s with 5% probability of exceedence



Safety Limit: 24m/s

Description	GEM Prob of Exceed %	Peak Gust m/s
<div></div> Criterion: Wind Comfort Standard for Walking Criterion (8m/s). Safety Limit (24m/s).	5%	24
<div></div> WD758-22 Proposed Massing Design and Awnings	2%	21
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Gust Equivalent Mean (m/s)	Maximum Gust (m/s)
10	15
15	25
20	35
25	45
30	55
35	65
40	75
45	85
50	95
55	105
60	115
65	125
70	135
75	145
80	155
85	165
90	175
95	185
100	195
105	205
110	215
115	225
120	235
125	245
130	255
135	265
140	275
145	285
150	295
155	305
160	315
165	325
170	335
175	345
180	355
185	365
190	375
195	385
200	395
205	405
210	415
215	425
220	435
225	445
230	455
235	465
240	475
245	485
250	495
255	505
260	515
265	525
270	535
275	545
280	555
285	565
290	575
295	585
300	595
305	605
310	615
315	625
320	635
325	645
330	655
335	665
340	675
345	685
350	695
355	705
360	715
365	725
370	735
375	745
380	755
385	765
390	775
395	785
400	795
405	805
410	815
415	825
420	835
425	845
430	855
435	865
440	875
445	885
450	895
455	905
460	915
465	925
470	935
475	945
480	955
485	965
490	975
495	985
500	995
505	1005
510	1015
515	1025
520	1035
525	1045
530	1055
535	1065
540	1075
545	1085
550	1095
555	1105
560	1115
565	1125
570	1135
575	1145
580	1155
585	1165
590	1175
595	1185
600	1195
605	1205
610	1215
615	1225
620	1235
625	1245
630	1255
635	1265
640	1275
645	1285
650	1295
655	1305
660	1315
665	1325
670	1335
675	1345
680	1355
685	1365
690	1375
695	1385
700	1395
705	1405
710	1415
715	1425
720	1435
725	1445
730	1455
735	1465
740	1475
745	1485
750	1495
755	1505
760	1515
765	1525
770	1535
775	1545
780	1555
785	1565
790	1575
795	1585
800	1595
805	1605
810	16



WD758-22 Blackwattle Bay, Sydney June 1, 2022

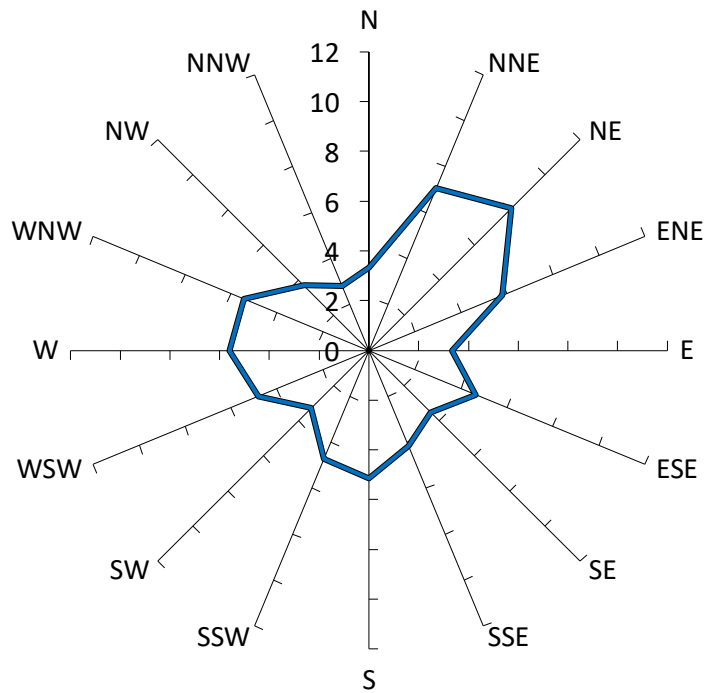
Gust Equivalent Mean (m/s)	Maximum Gust (m/s)
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Description		GEM Prob of Exceed %	Peak Gust m/s
	Criterion: Wind Comfort Standard for Walking Criterion (8m/s). Safety Limit (24m/s).	5%	24
	WD758-22 Proposed Massing Design and Awnings	1%	20

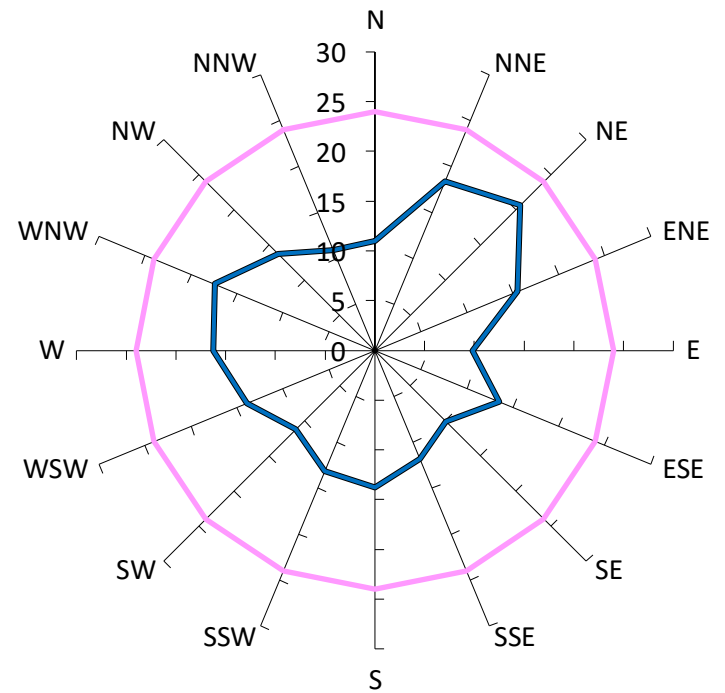
Results for P59

Gust Equivalent Mean (m/s)



Comfort Criteria: 8m/s with 5% probability of exceedence

Maximum Gust (m/s)

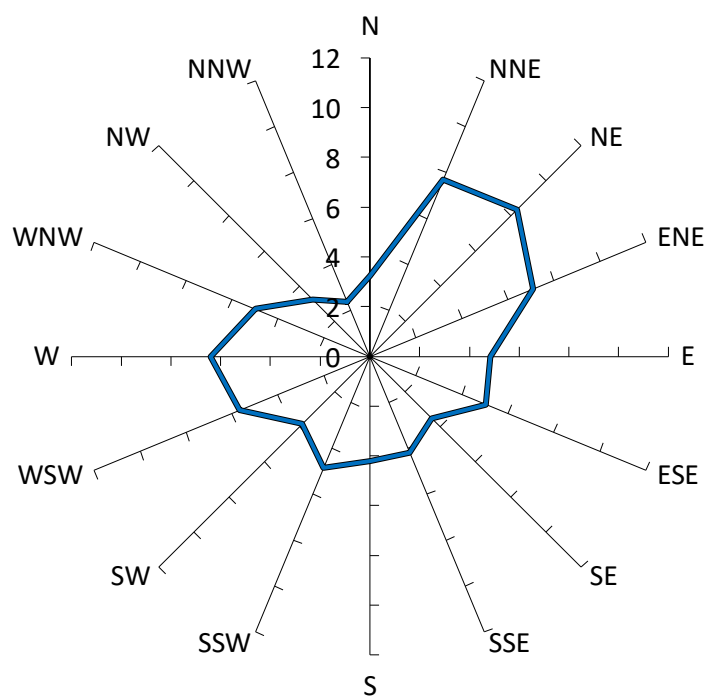


Safety Limit: 24m/s

[illegible]

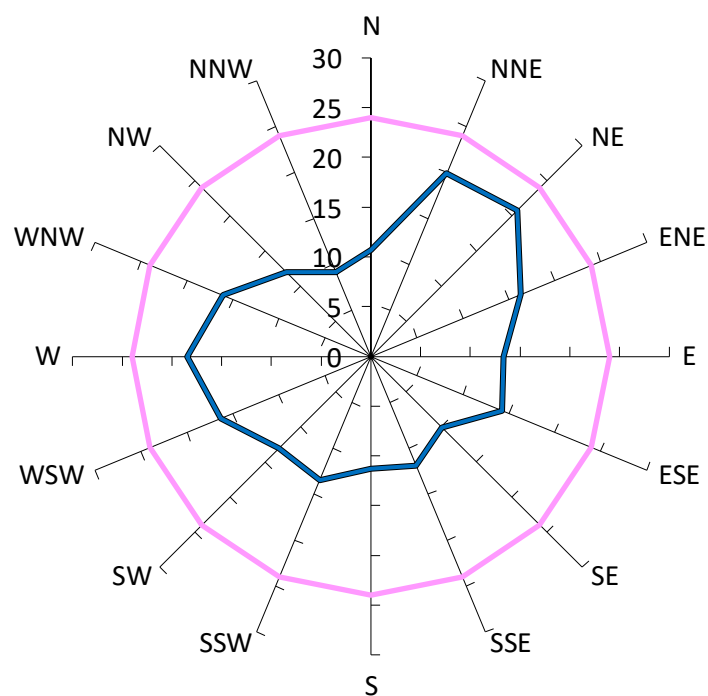
Results for P60

Gust Equivalent Mean (m/s)











Comfort Criteria: 8m/s with 5% probability of exceedence

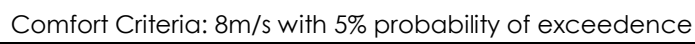
Maximum Gust (m/s)



Safety Limit: 24m/s

Description		GEM Prob of Exceed %	Peak Gust m/s
	Criterion: Wind Comfort Standard for Walking Criterion (8m/s). Safety Limit (24m/s).	5%	24
	WD758-22 Proposed Massing Design and Awnings	3%	21
			
			
			
			
			
			

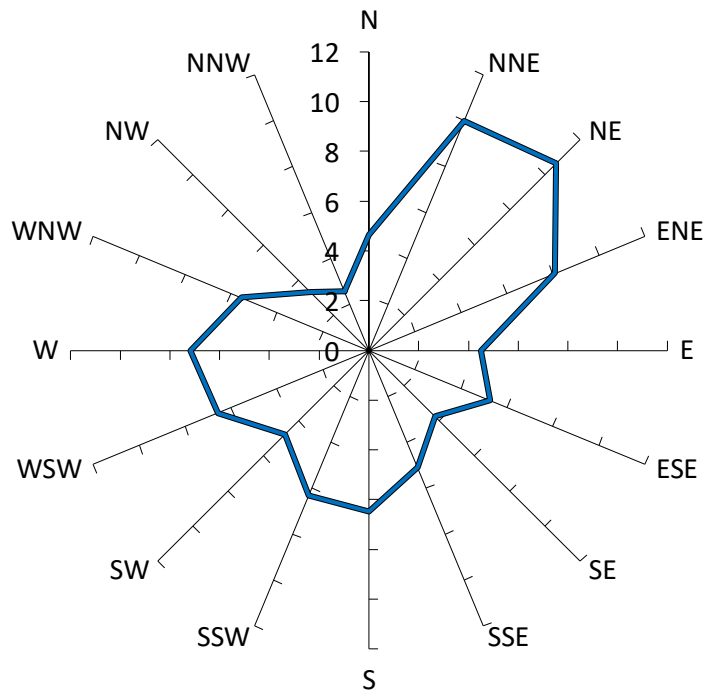
Gust Equivalent Mean (m/s)	Maximum Gust (m/s)
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WD758-22 Blackwattle Bay, Sydney June 1, 2022

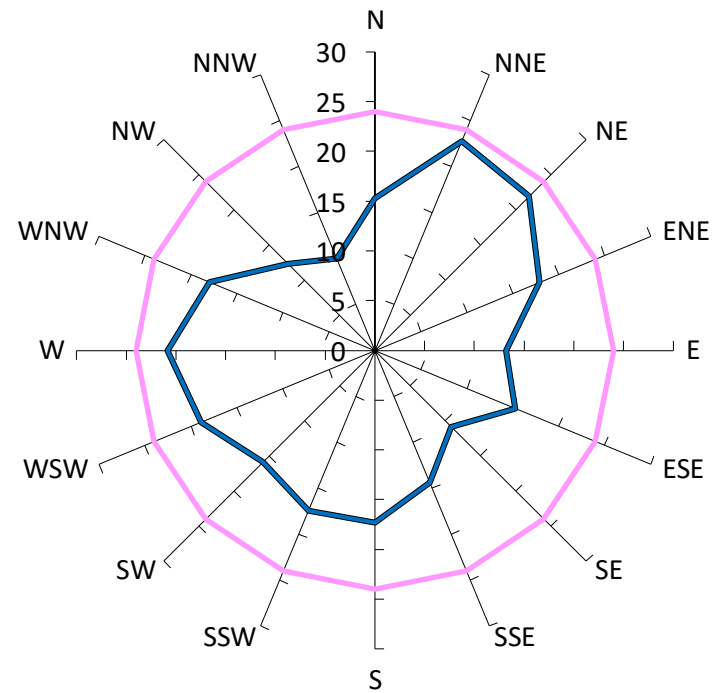
Results for P62

Gust Equivalent Mean (m/s)



Comfort Criteria: 8m/s with 5% probability of exceedence

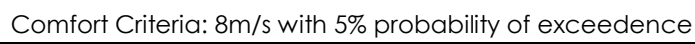
Maximum Gust (m/s)



Safety Limit: 24m/s

[illegible]

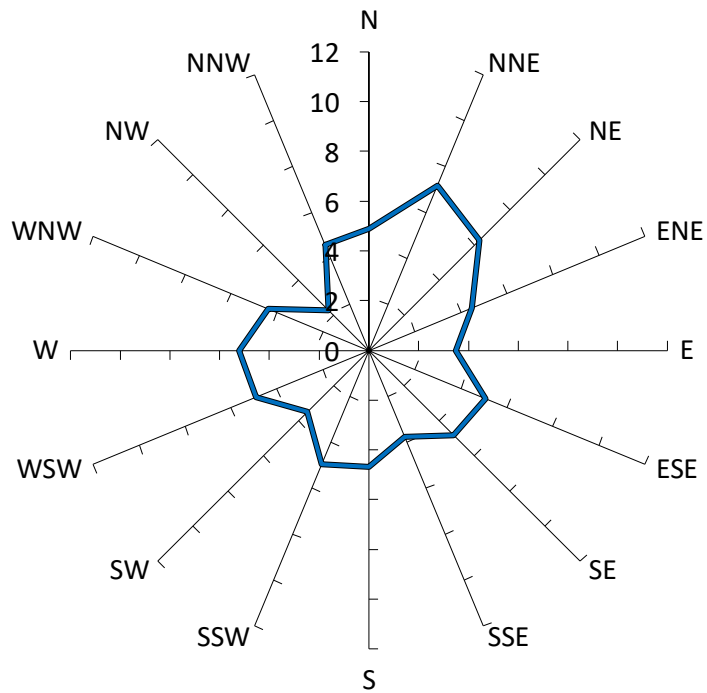
Gust Equivalent Mean (m/s)	Maximum Gust (m/s)
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WD758-22 Blackwattle Bay, Sydney June 1, 2022

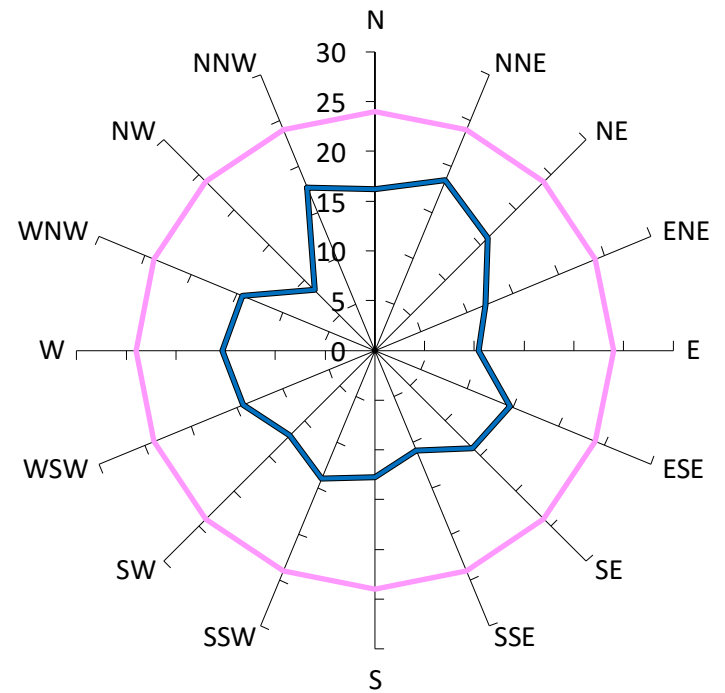
Results for P64

Gust Equivalent Mean (m/s)



Comfort Criteria: 8m/s with 5% probability of exceedence

Maximum Gust (m/s)



Safety Limit: 24m/s

[illegible]

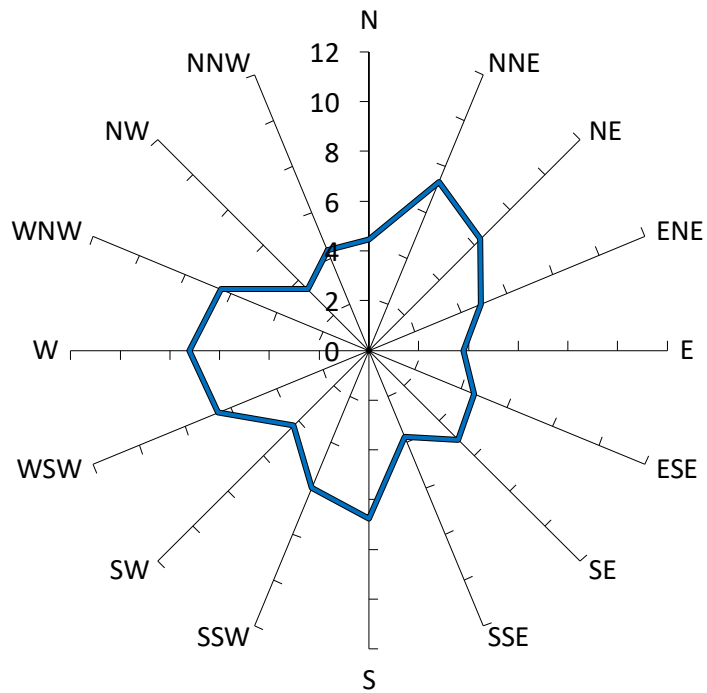
Gust Equivalent Mean (m/s)	Maximum Gust (m/s)
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WD758-22 Blackwattle Bay, Sydney June 1, 2022

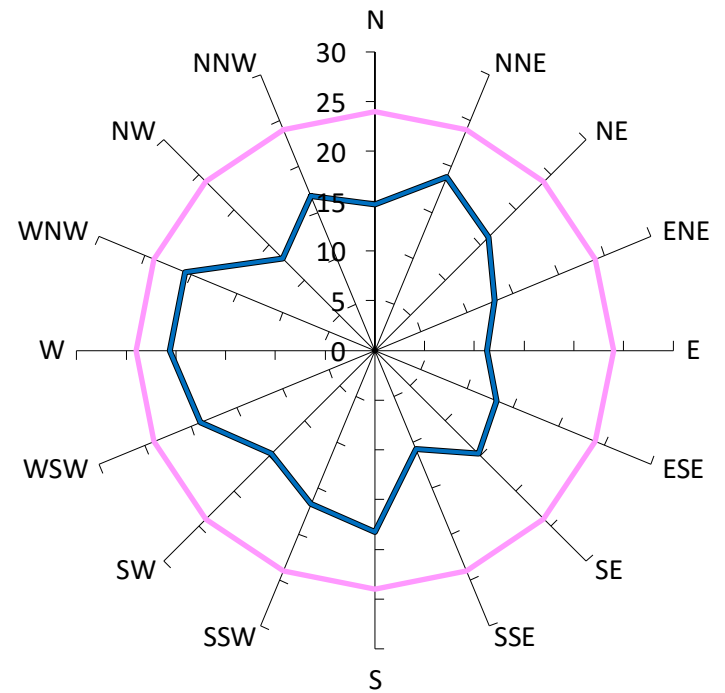
Results for P66

Gust Equivalent Mean (m/s)



Comfort Criteria: 8m/s with 5% probability of exceedence

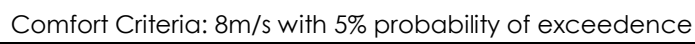
Maximum Gust (m/s)



Safety Limit: 24m/s

[illegible]

Gust Equivalent Mean (m/s)	Maximum Gust (m/s)
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WD758-22 Blackwattle Bay, Sydney June 1, 2022

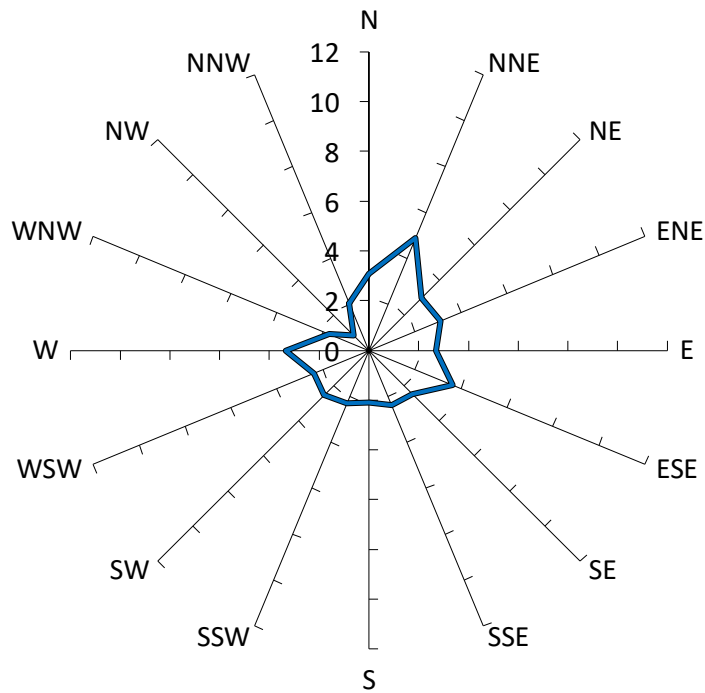
Gust Equivalent Mean (m/s)	Maximum Gust (m/s)
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Item	Percentage	Count
Criterion: Wind Comfort Standard for Walking Criterion (8m/s). Safety Limit (24m/s).	5%	24
WD758-22 Proposed Massing Design and Awnings	11%	24

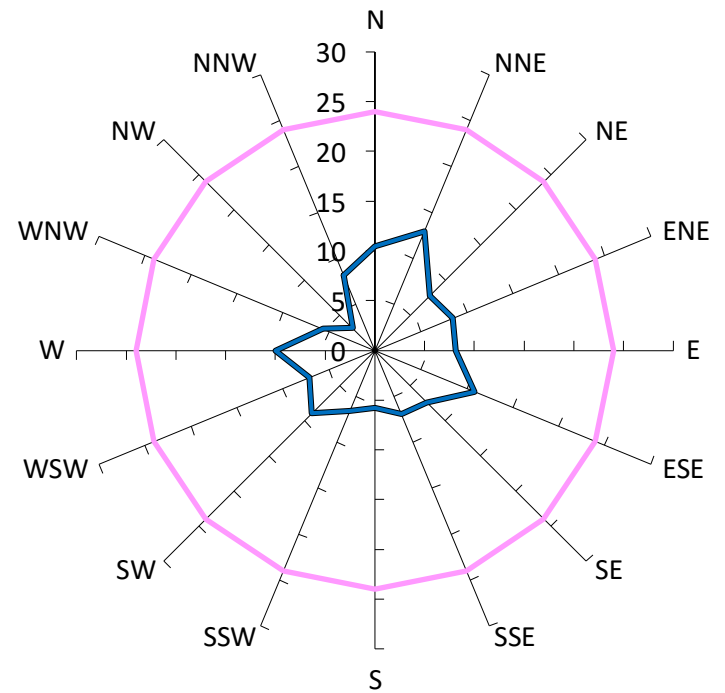
Results for P69

Gust Equivalent Mean (m/s)



Comfort Criteria: 8m/s with 5% probability of exceedence

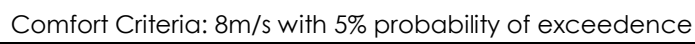
Maximum Gust (m/s)



Safety Limit: 24m/s

[illegible]

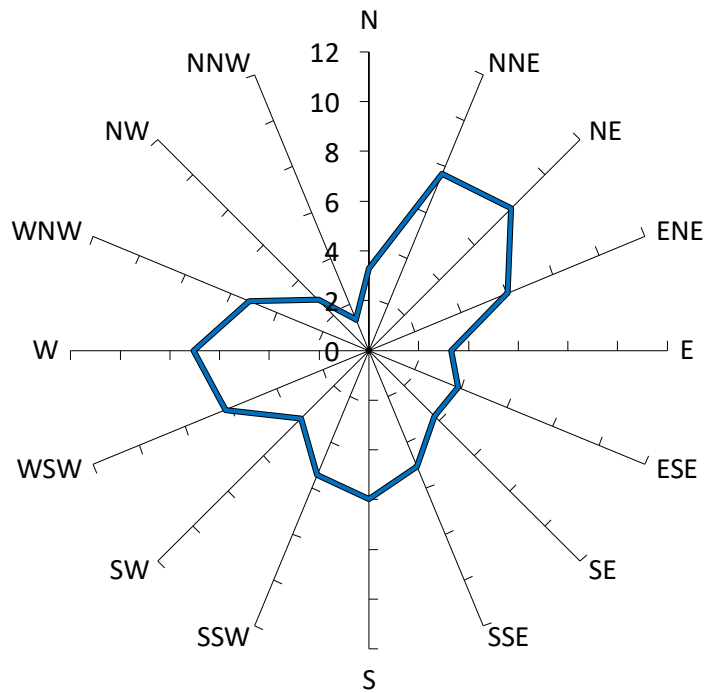
Gust Equivalent Mean (m/s)	Maximum Gust (m/s)
10	15
15	25
20	35
25	45
30	55
35	65
40	75
45	85
50	95
55	105
60	115
65	125
70	135
75	145
80	155
85	165
90	175
95	185
100	195
105	205
110	215
115	225
120	235
125	245
130	255
135	265
140	275
145	285
150	295
155	305
160	315
165	325
170	335
175	345
180	355
185	365
190	375
195	385
200	395
205	405
210	415
215	425
220	435
225	445
230	455
235	465
240	475
245	485
250	495
255	505
260	515
265	525
270	535
275	545
280	555
285	565
290	575
295	585
300	595
305	605
310	615
315	625
320	635
325	645
330	655
335	665
340	675
345	685
350	695
355	705
360	715
365	725
370	735
375	745
380	755
385	765
390	775
395	785
400	795
405	805
410	815
415	825
420	835
425	845
430	855
435	865
440	875
445	885
450	895
455	905
460	915
465	925
470	935
475	945
480	955
485	965
490	975
495	985
500	995
505	1005
510	1015
515	1025
520	1035
525	1045
530	1055
535	1065
540	1075
545	1085
550	1095
555	1105
560	1115
565	1125
570	1135
575	1145
580	1155
585	1165
590	1175
595	1185
600	1195
605	1205
610	1215
615	1225
620	1235
625	1245
630	1255
635	1265
640	1275
645	1285
650	1295
655	1305
660	1315
665	1325
670	1335
675	1345
680	1355
685	1365
690	1375
695	1385
700	1395
705	1405
710	1415
715	1425
720	1435
725	1445
730	1455
735	1465
740	1475
745	1485
750	1495
755	1505
760	1515
765	1525
770	1535
775	1545
780	1555
785	1565
790	1575
795	1585
800	1595
805	1605
810	16



WD758-22 Blackwattle Bay, Sydney June 1, 2022

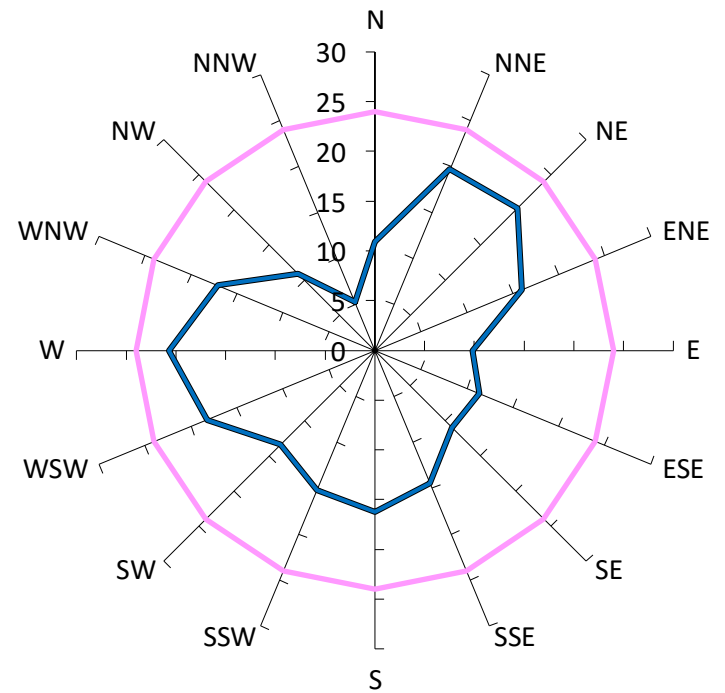
Results for P71

Gust Equivalent Mean (m/s)



Comfort Criteria: 8m/s with 5% probability of exceedence

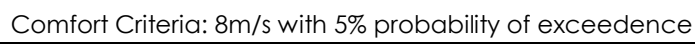
Maximum Gust (m/s)



Safety Limit: 24m/s

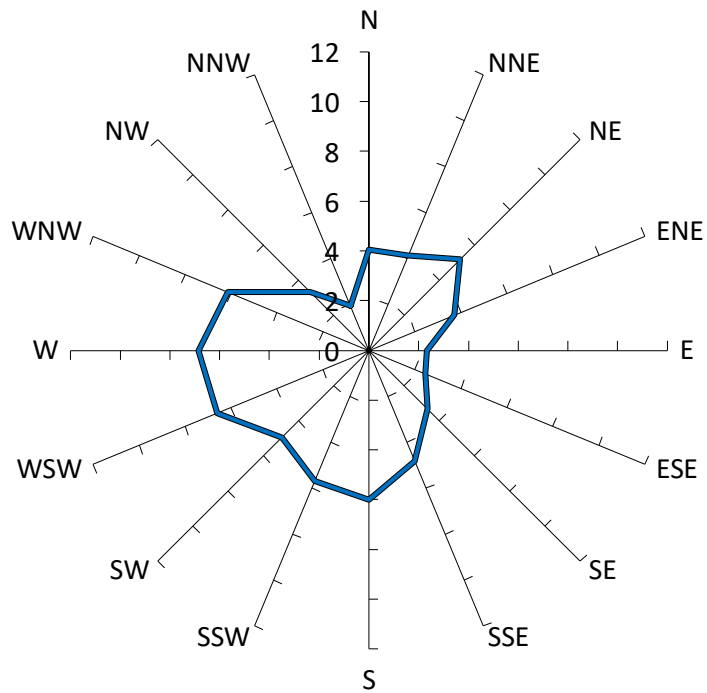
[illegible]

Gust Equivalent Mean (m/s)	Maximum Gust (m/s)
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[illegible]

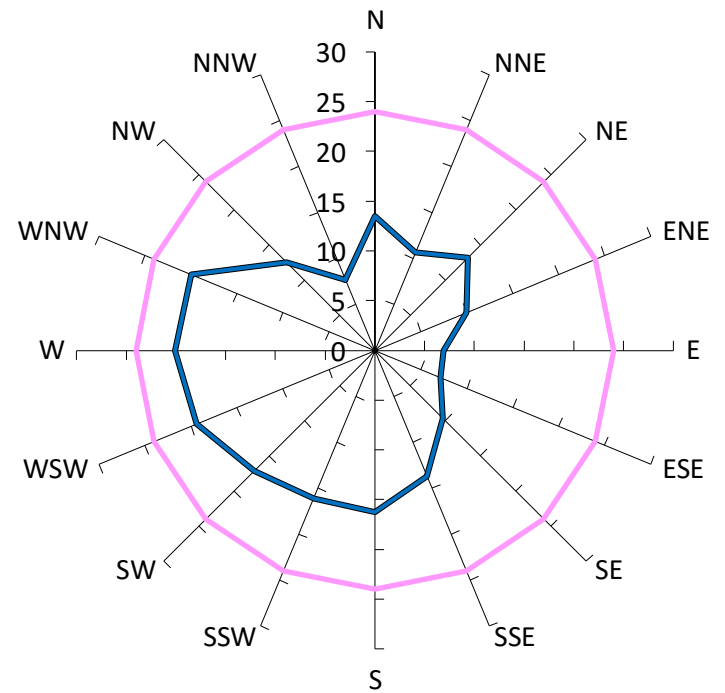
Results for P73

Gust Equivalent Mean (m/s)



Comfort Criteria: 8m/s with 5% probability of exceedence

Maximum Gust (m/s)

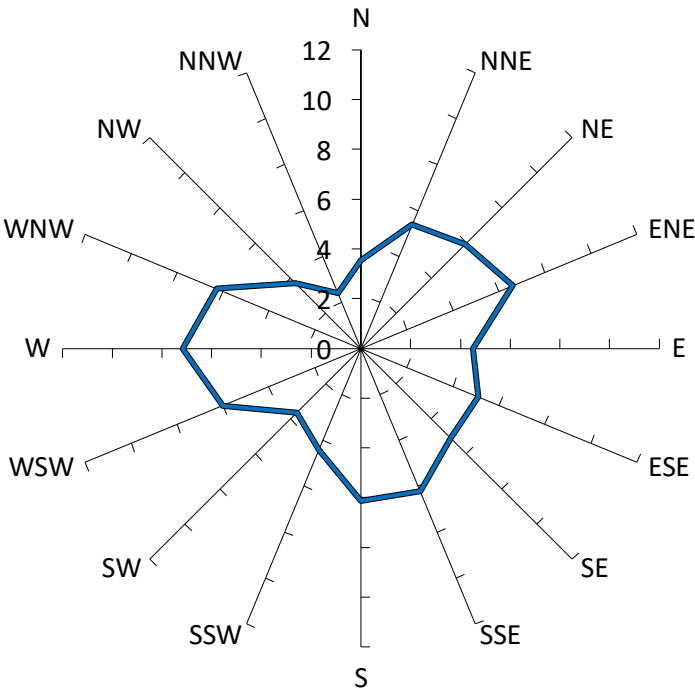


Safety Limit: 24m/s

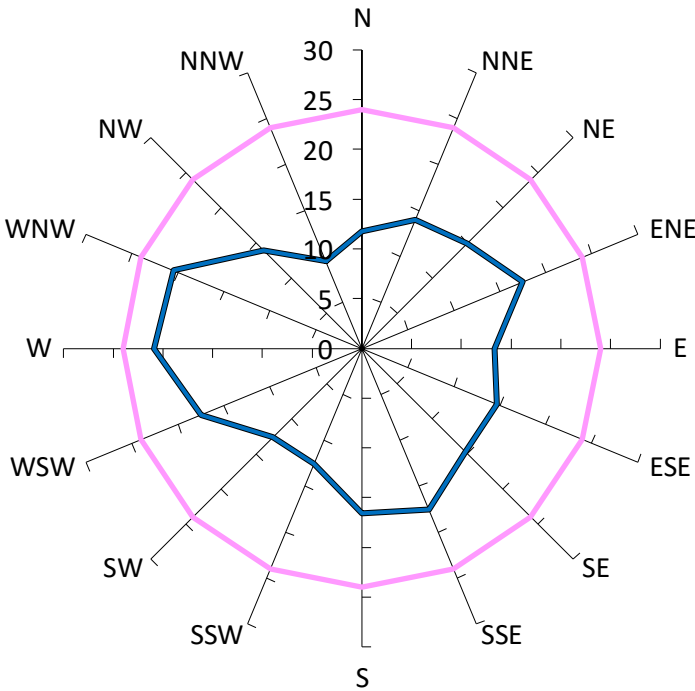
[illegible]

Results for P74

Gust Equivalent Mean (m/s)	Maximum Gust (m/s)
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Comfort Criteria: 8m/s with 5% probability of exceedence

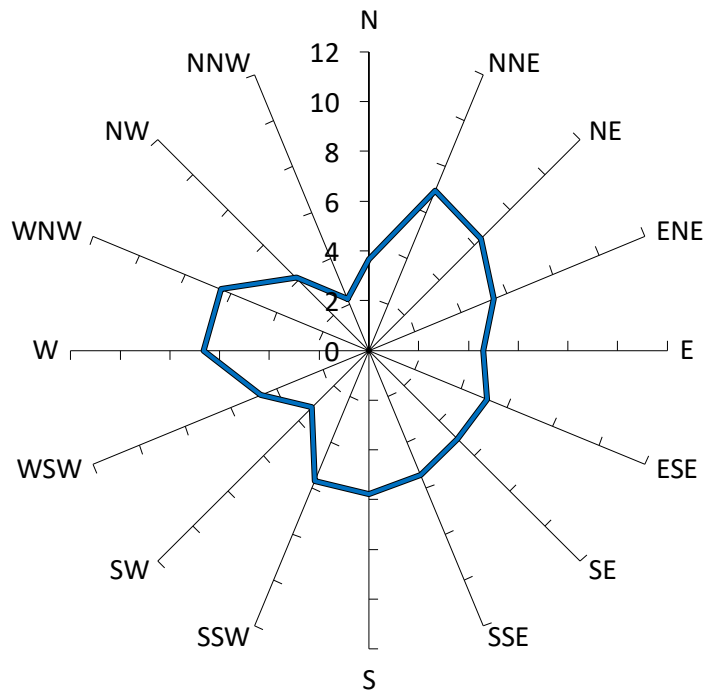


Safety Limit: 24m/s

Description	GEM Prob of Exceed %	Peak Gust m/s
<div></div> Criterion: Wind Comfort Standard for Walking Criterion (8m/s). Safety Limit (24m/s).	5%	24
<div></div> WD758-22 Proposed Massing Design and Awnings	2%	21
<div></div>		
<div></div>		
<div></div>		
<div></div>		
<div></div>		
<div></div>		
<div></div>		
<div></div>		
<div></div>		
<div></div>		

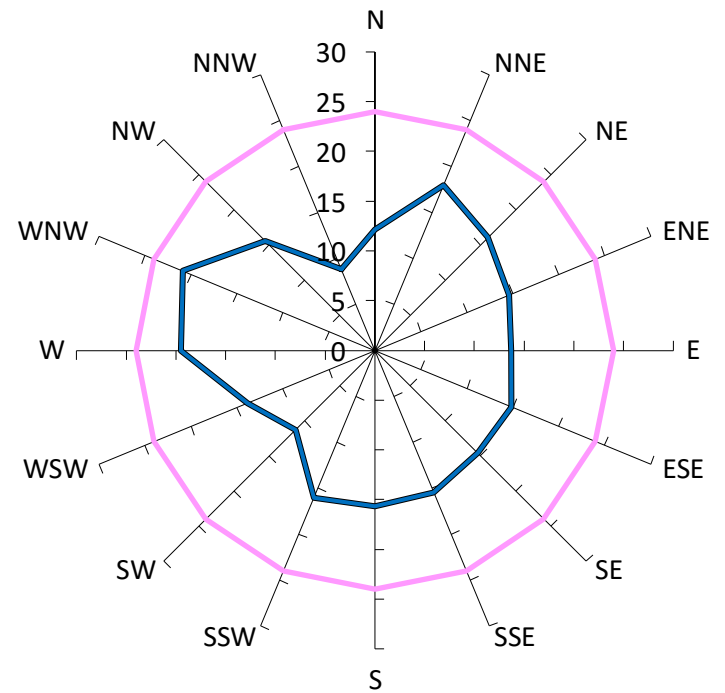
Results for P75

Gust Equivalent Mean (m/s)



Comfort Criteria: 8m/s with 5% probability of exceedence

Maximum Gust (m/s)

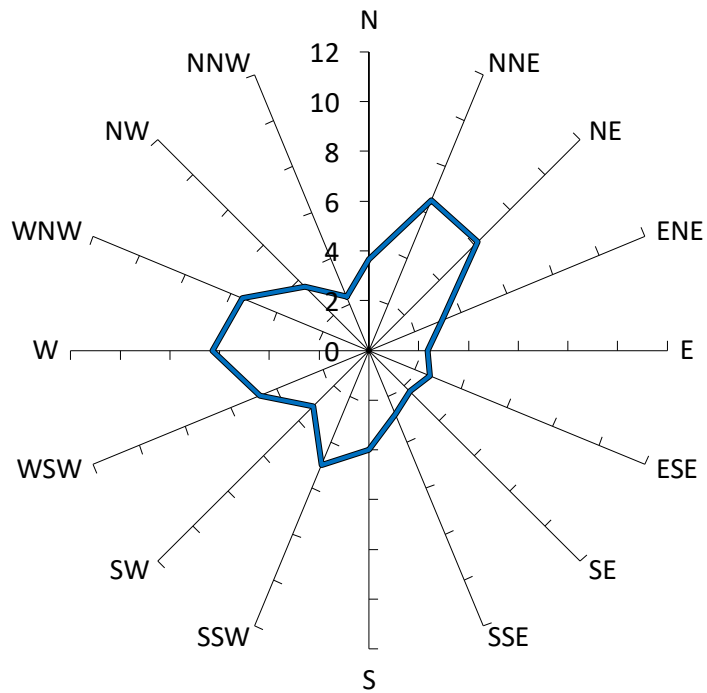


Safety Limit: 24m/s

[illegible]

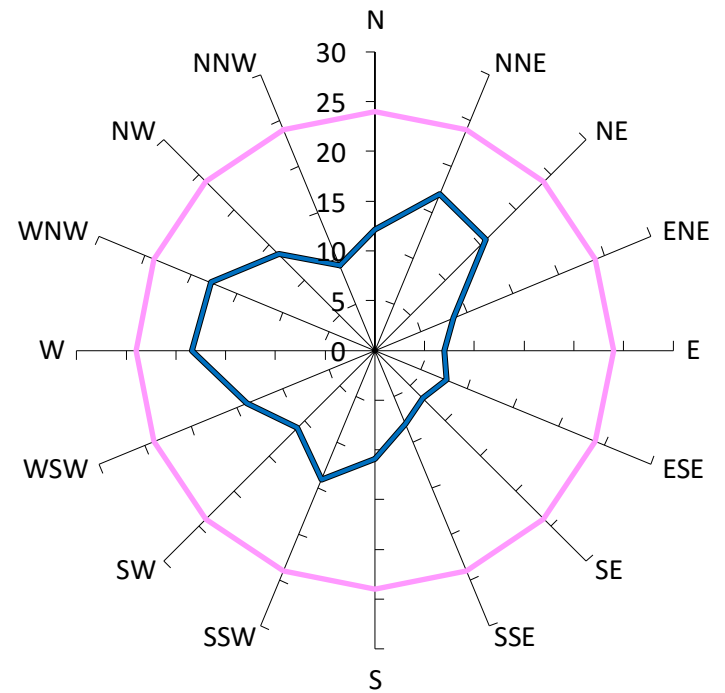
Results for P76

Gust Equivalent Mean (m/s)



Comfort Criteria: 8m/s with 5% probability of exceedence

Maximum Gust (m/s)

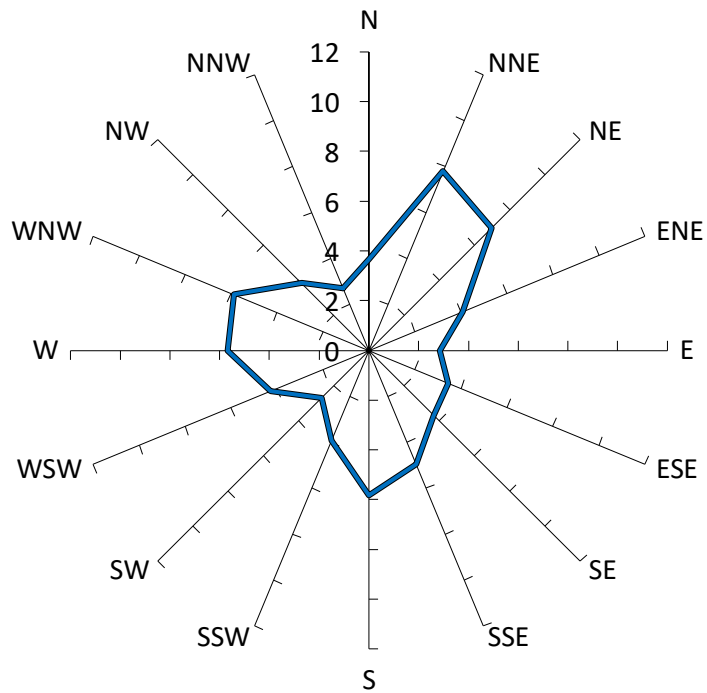


Safety Limit: 24m/s

[illegible]

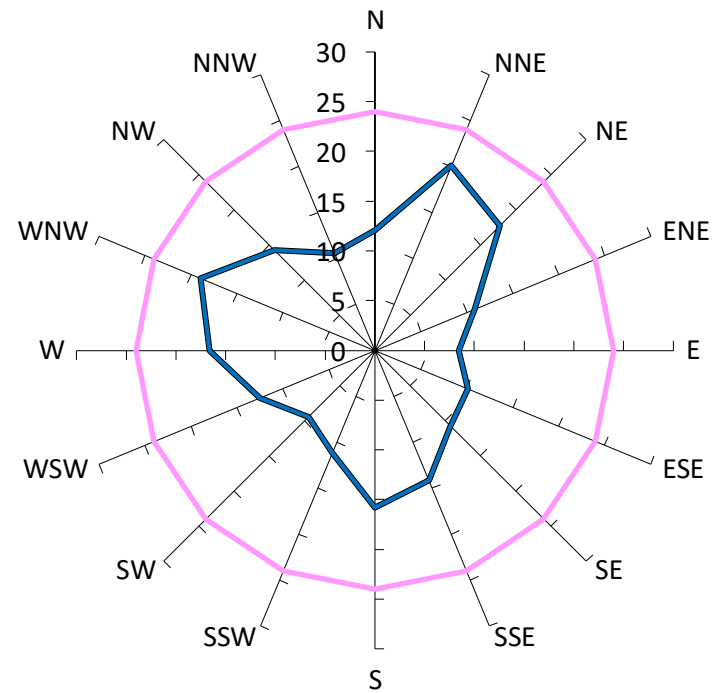
Results for P77

Gust Equivalent Mean (m/s)



Comfort Criteria: 8m/s with 5% probability of exceedence

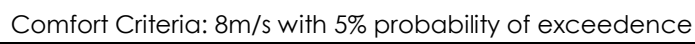
Maximum Gust (m/s)



Safety Limit: 24m/s

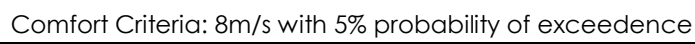
[illegible]

Gust Equivalent Mean (m/s)	Maximum Gust (m/s)
10	15
15	25
20	35
25	45
30	55
35	65
40	75
45	85
50	95
55	105
60	115
65	125
70	135
75	145
80	155
85	165
90	175
95	185
100	195
105	205
110	215
115	225
120	235
125	245
130	255
135	265
140	275
145	285
150	295
155	305
160	315
165	325
170	335
175	345
180	355
185	365
190	375
195	385
200	395
205	405
210	415
215	425
220	435
225	445
230	455
235	465
240	475
245	485
250	495
255	505
260	515
265	525
270	535
275	545
280	555
285	565
290	575
295	585
300	595
305	605
310	615
315	625
320	635
325	645
330	655
335	665
340	675
345	685
350	695
355	705
360	715
365	725
370	735
375	745
380	755
385	765
390	775
395	785
400	795
405	805
410	815
415	825
420	835
425	845
430	855
435	865
440	875
445	885
450	895
455	905
460	915
465	925
470	935
475	945
480	955
485	965
490	975
495	985
500	995
505	1005
510	1015
515	1025
520	1035
525	1045
530	1055
535	1065
540	1075
545	1085
550	1095
555	1105
560	1115
565	1125
570	1135
575	1145
580	1155
585	1165
590	1175
595	1185
600	1195
605	1205
610	1215
615	1225
620	1235
625	1245
630	1255
635	1265
640	1275
645	1285
650	1295
655	1305
660	1315
665	1325
670	1335
675	1345
680	1355
685	1365
690	1375
695	1385
700	1395
705	1405
710	1415
715	1425
720	1435
725	1445
730	1455
735	1465
740	1475
745	1485
750	1495
755	1505
760	1515
765	1525
770	1535
775	1545
780	1555
785	1565
790	1575
795	1585
800	1595
805	1605
810	16



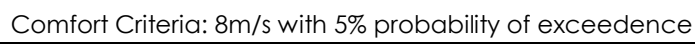
WD758-22 Blackwattle Bay, Sydney June 1, 2022








Gust Equivalent Mean (m/s)	Maximum Gust (m/s)
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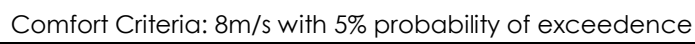
WD758-22 Blackwattle Bay, Sydney June 1, 2022

Gust Equivalent Mean (m/s)	Maximum Gust (m/s)
----------------------------	--------------------



Description		GEM Prob of Exceed %	Peak Gust m/s
	Criterion: Wind Comfort Standard for Walking Criterion (8m/s). Safety Limit (24m/s).	5%	24
	WD758-22 Proposed Massing Design and Awnings	< 1%	11
			
			
			
			
			
			

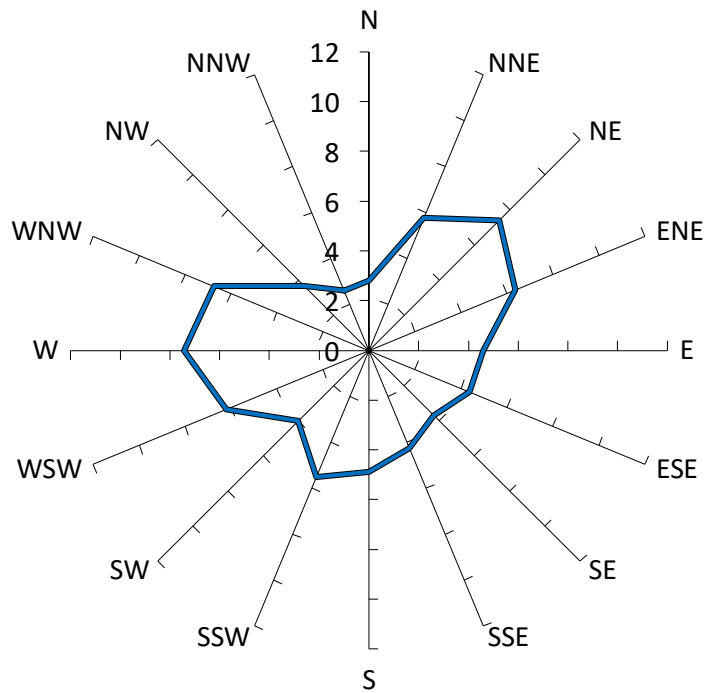
Gust Equivalent Mean (m/s)	Maximum Gust (m/s)
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WD758-22 Blackwattle Bay, Sydney June 1, 2022

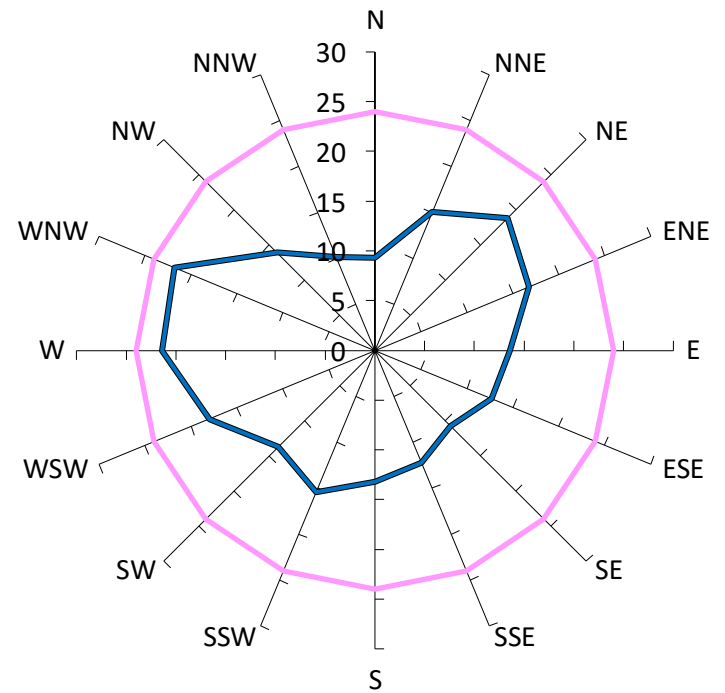
Results for P82

Gust Equivalent Mean (m/s)



Comfort Criteria: 8m/s with 5% probability of exceedence

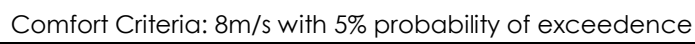
Maximum Gust (m/s)









Safety Limit: 24m/s

[illegible]

Gust Equivalent Mean (m/s)	Maximum Gust (m/s)
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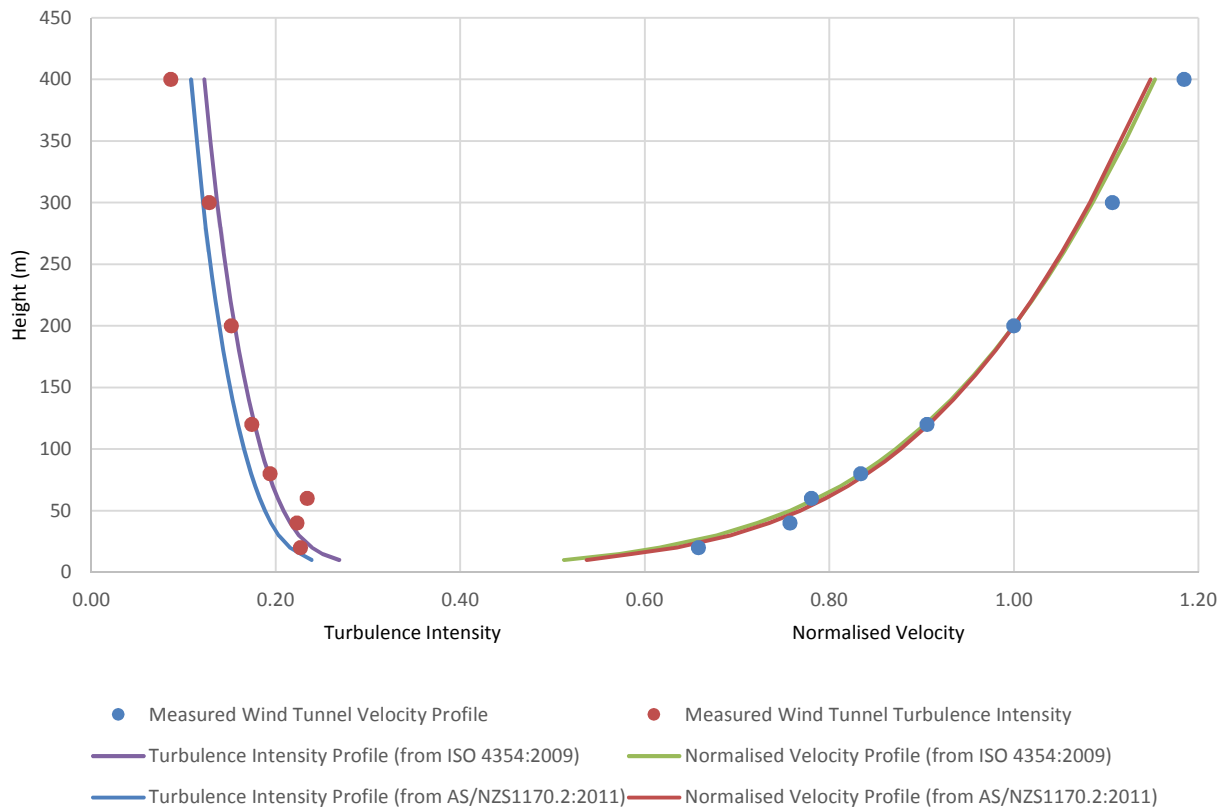


Description		GEM Prob of Exceed %	Peak Gust m/s
	Criterion: Wind Comfort Standard for Walking Criterion (8m/s). Safety Limit (24m/s).	5%	24
	WD758-22 Proposed Massing Design and Awnings	4%	22
			
			
			
			
			
			



APPENDIX D VELOCITY AND TURBULENCE INTENSITY PROFILES

Mean Velocity and Turbulence Intensity for Suburban/Forest Terrain ($0.2\text{m} < z_0 < 0.3\text{m}$) (TC3) at a 1:400 Scale



Longitudinal Spectra Density for Suburban/Forest Terrain ($0.2\text{m} < z_0 < 0.3\text{m}$) (TC3) at a 1:400 Scale

